

# Homogeneous Charge Compression Ignition (HCCI)

Dual fuel HCCI combustion

- High octane and high cetane number fuels -

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## 1) Previous study ---- HCCI

a) HCCI combustion of DME: Spectrum analysis of chemiluminescence was performed in an HCCI engine.

(SAE Paper, No.2003-01-1828)

Nobuyuki Kawahara, Eiji Tomita, Hisashi Kagajo

b) Ion Current Measurement in a Homogeneous Charge Compression Ignition Engine,

International Journal of Engine Research, Vol.6, (2005), pp.453-463.

Tatsuya Tanaka, Kazuaki Narahara, Michihiko Tabata, Sadami Yoshiyama and Eiji Tomita

----- gasoline based HCCI

c) Dual fuel HCCI:

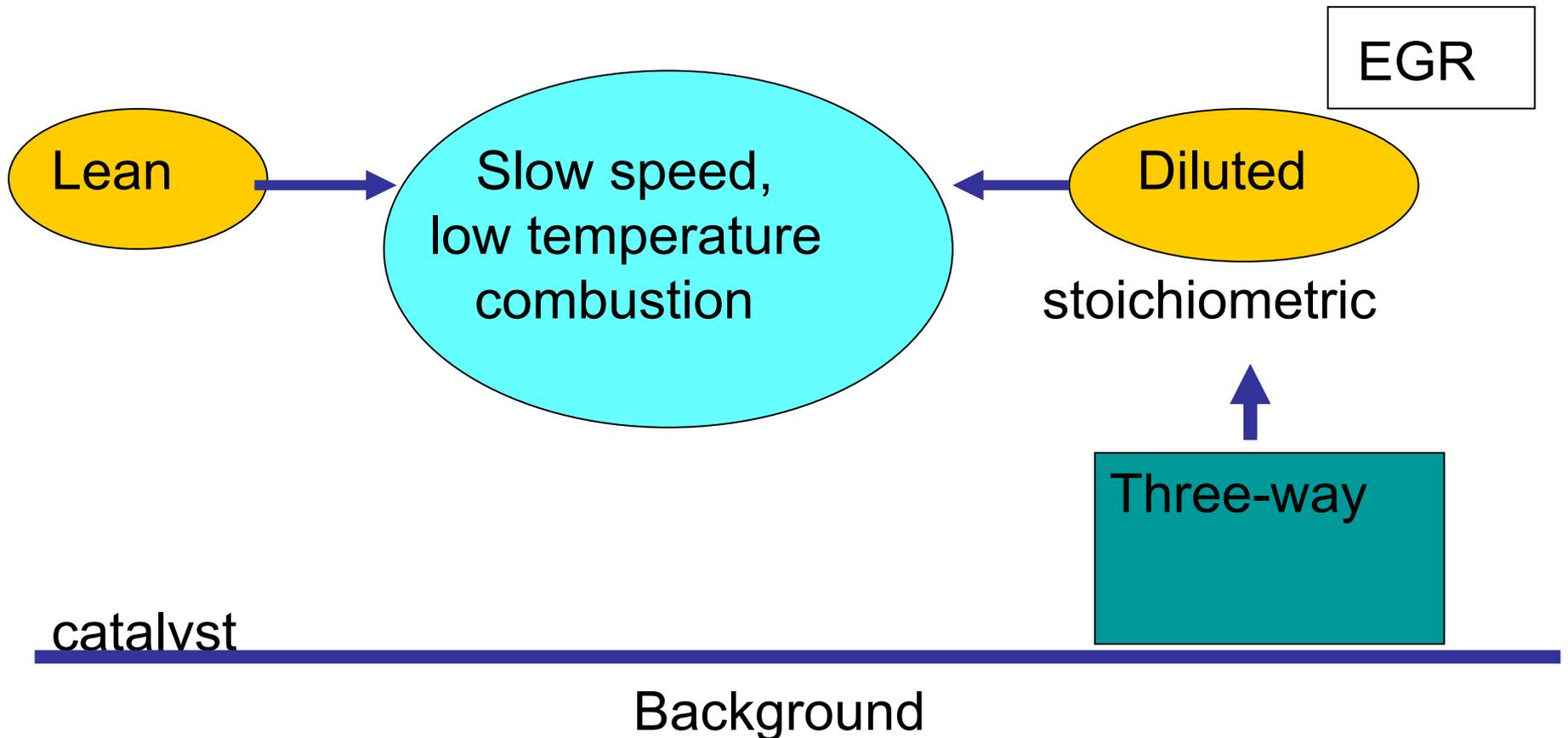
- \* Hydrogen is induced from intake port and gas oil is injected into the cylinder and combustion characteristics and exhaust emissions were investigated.  
(SAE Paper, No.2001-01-3503)

- \* Methane is induced from intake port and gas oil is injected into the cylinder and combustion characteristics and exhaust emissions were investigated. The effect of diluted gas was also investigated. The high dilution condition enables stoichiometric combustion with no smoke and very low NO<sub>x</sub>.  
(SAE Paper, No.2002-01-2723)  
(HCCI symposium in Berkeley, 2004)

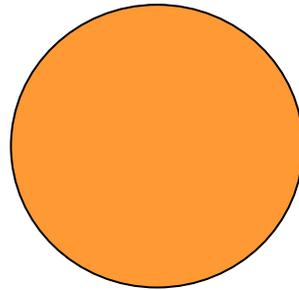
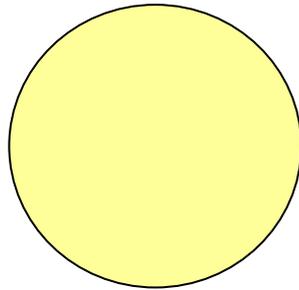
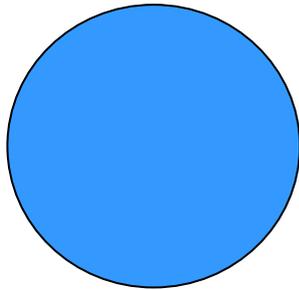
Demand from the society

- Increasing thermal efficiency (reducing CO<sub>2</sub>)
- Reducing pollutant emissions

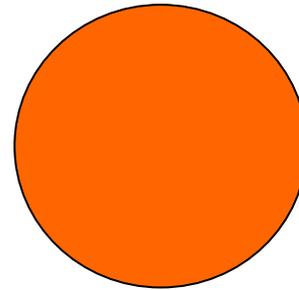
HCCI : low NO<sub>x</sub>, no smoke : new Diesel



Unburned



Burned



Time

-No smoke, Low NOx

-Problems to be solved

\* Ignition control under transient operation

Temperature, pressure and concentration of fuel, EGR

Variable valve timing

\* Higher load without knock

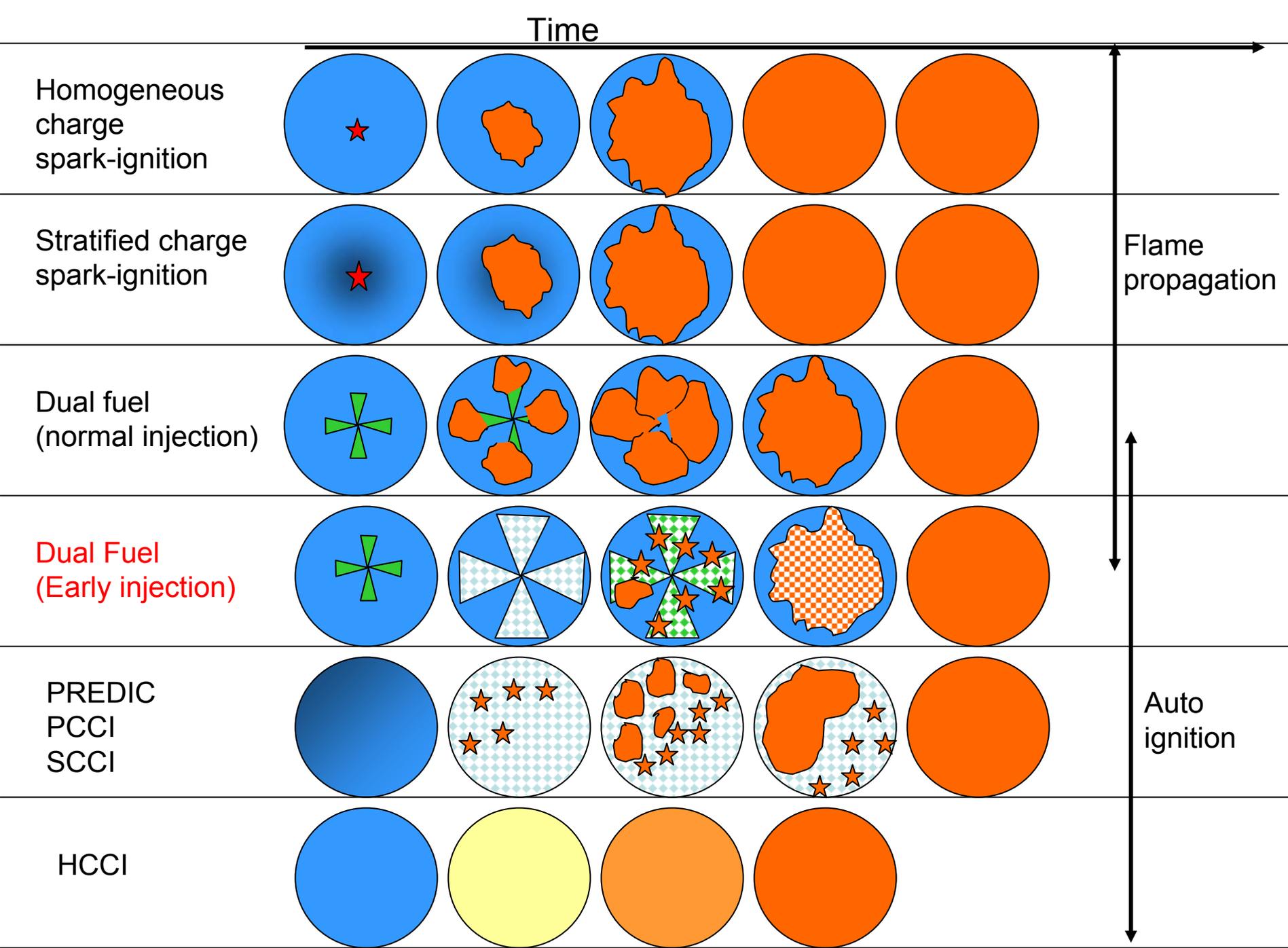
Degree of stratification ←

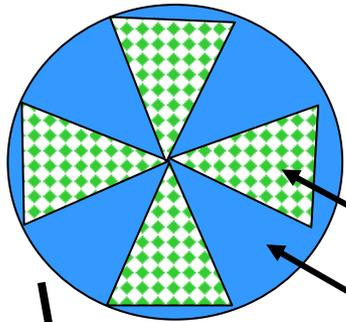
\* how to supply the fuel

\* in-cylinder flow

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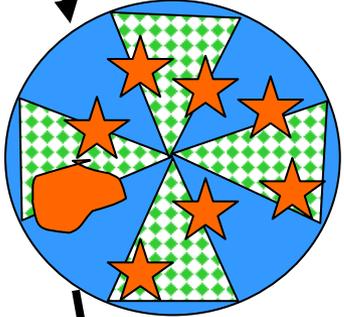
Homogeneous Charge Compression Ignition combustion



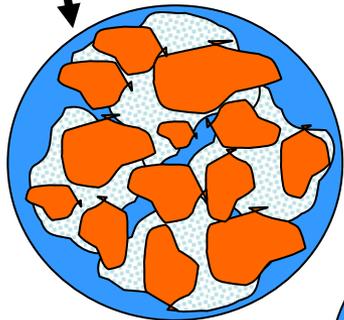


Fuel injected is dispersed widely without ignition because of early injection.

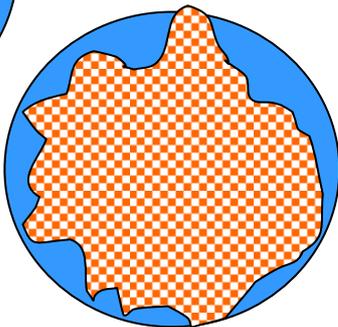
High cetane number fuel for ignition source  
High octane number fuel



No fuel-rich region leads to no smoke.  
No high temperature region leads to less NOx.



The lean fuel surrounded with burned gas of high cetane number fuel is expected to be burned.



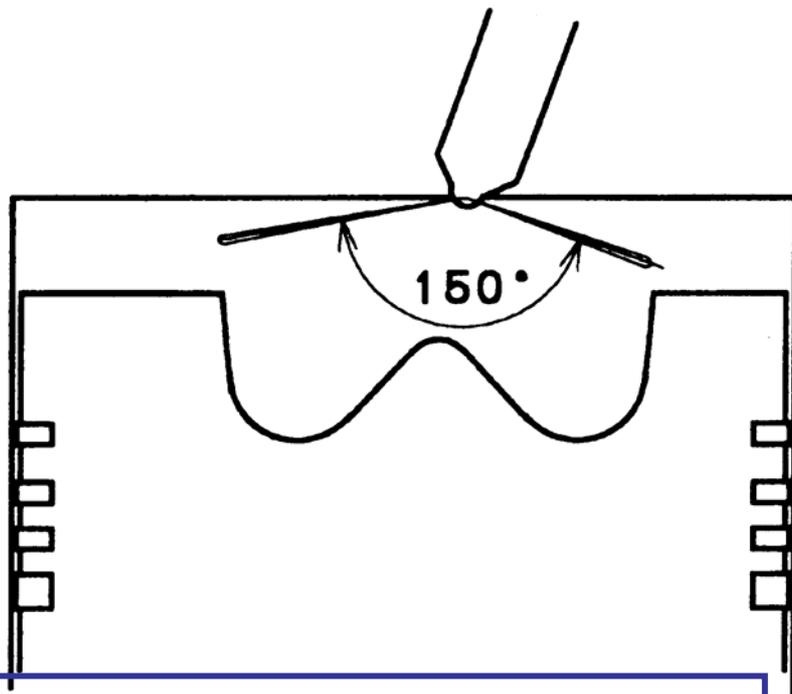
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Concept of this study

- Dual fuel engine (**methane + diesel fuel**)  
combination of **high octane number fuel** & **high cetane number fuel** using a DI diesel engine
- Early injection (**40-50 deg.BTDC**) : HCCI concept  
low NO<sub>x</sub>, no smoke  
but rapid combustion with high NO<sub>x</sub> in high load
- EGR (**N<sub>2</sub>-dilution**)  
achieving mild combustion in high load
- Stoichiometric combustion
- ROHR and Exhaust emissions

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Experimental method



Single cylinder,  
4 stroke cycle

Direct injection (diesel fuel)  
+ induction from intake port  
(methane)

Bore x stroke: 92 x 96 mm  
Displacement: 638 cm<sup>3</sup>

Engine speed:  $n = 1000 \text{ rpm}$

Injection timing:

$\theta_{inj} = \text{TDC} \sim 50 \text{ deg. BTDC}$

Equivalence ratio:

$\phi_t = 0.4 \sim 1.1$

N<sub>2</sub> dilution ratio:  $\alpha = 0 \sim 37.5\%$

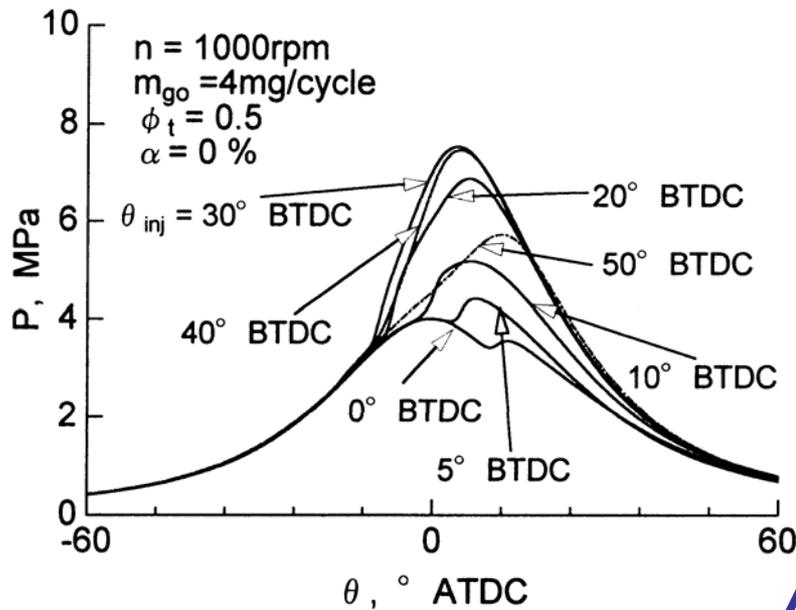
Compression ratio: 17.7:1

Injector: 4 holes ( $\phi$  0.26mm),

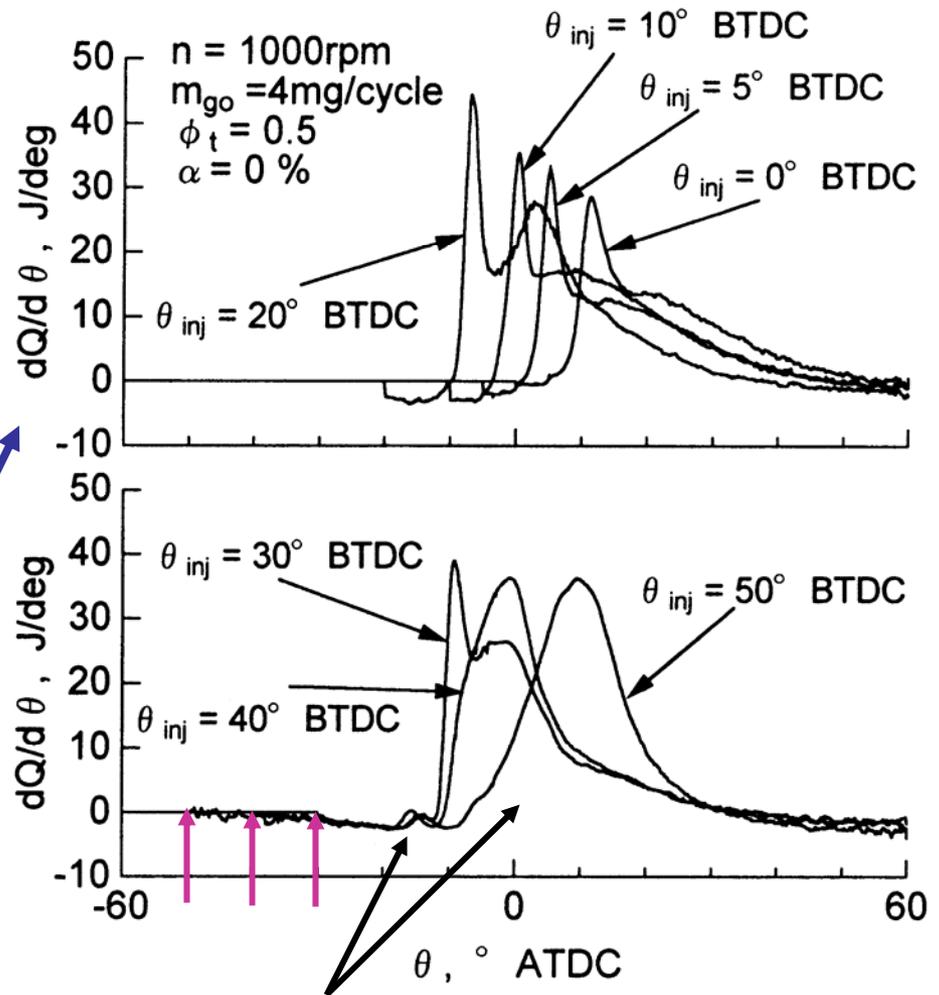
Spray angle: 150°

Combustion chamber: Deep dish

Engine specifications and combustion chamber

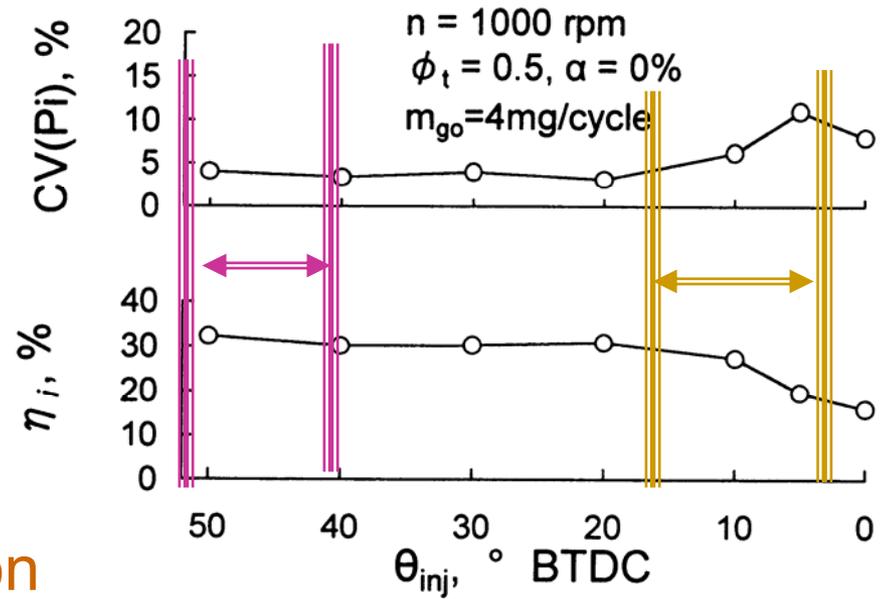
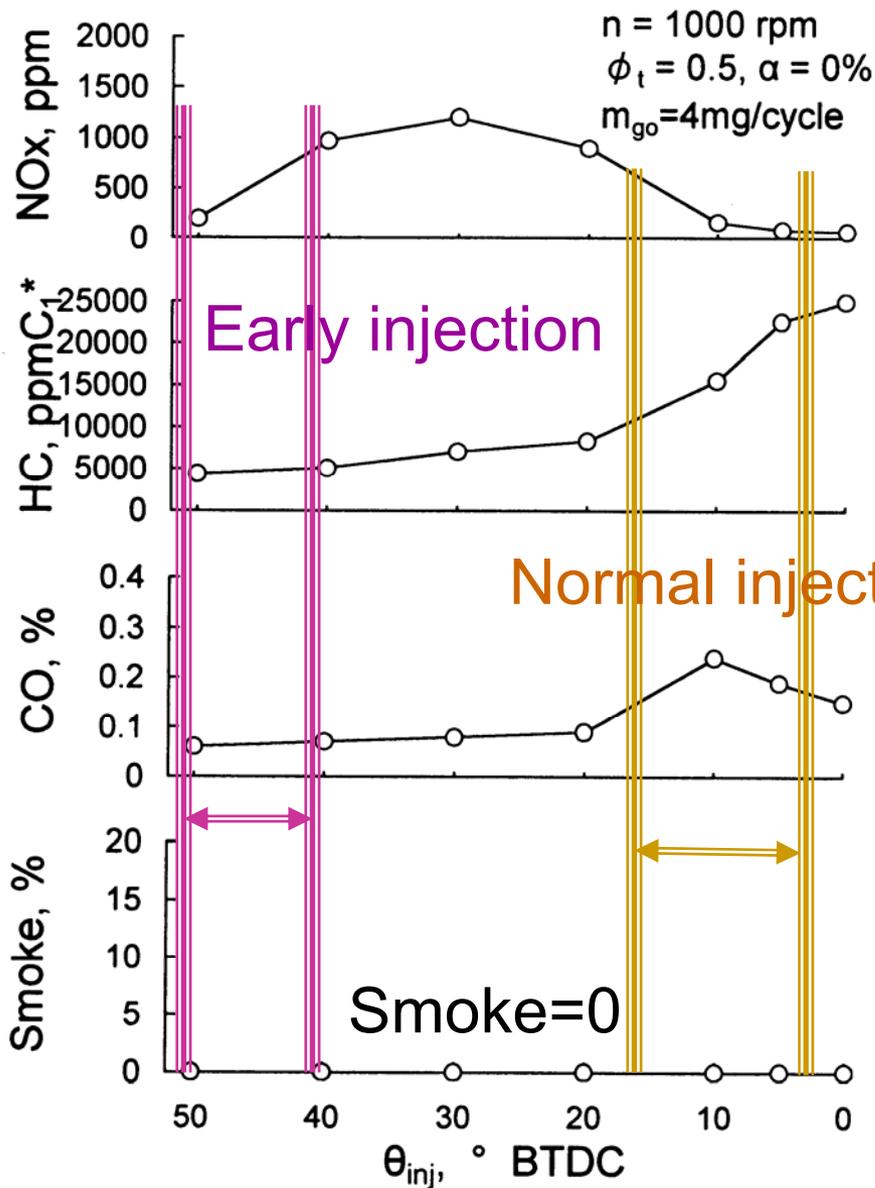


Normal injection  
 ( $\theta_{inj} = 0 \sim 20 \text{ deg. BTDC}$ )  
 Early injection  
 ( $\theta_{inj} = 30 \sim 50 \text{ deg. BTDC}$ )



Low temperature reaction due to diesel fuel  
 One large peak with retarded combustion

Pressure and ROHR without  $\text{N}_2$ -dilution ( $\alpha = 0\%$ )

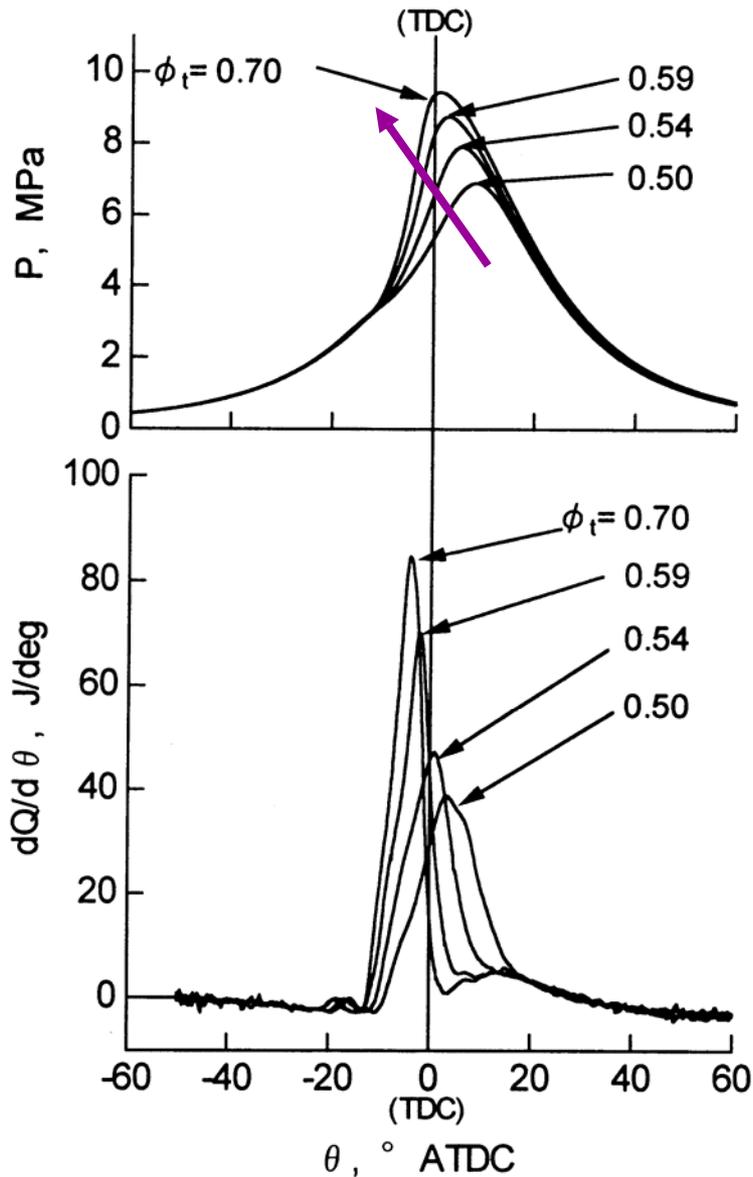


$\phi_t = 0.5$

**Early injection**

- Low NOx, low HC, Low CO
- Low cycle-to-cycle fluctuation
- High thermal efficiency

Exhaust emissions and thermal efficiency w/o N<sub>2</sub>-dilution ( $\alpha=0\%$ )

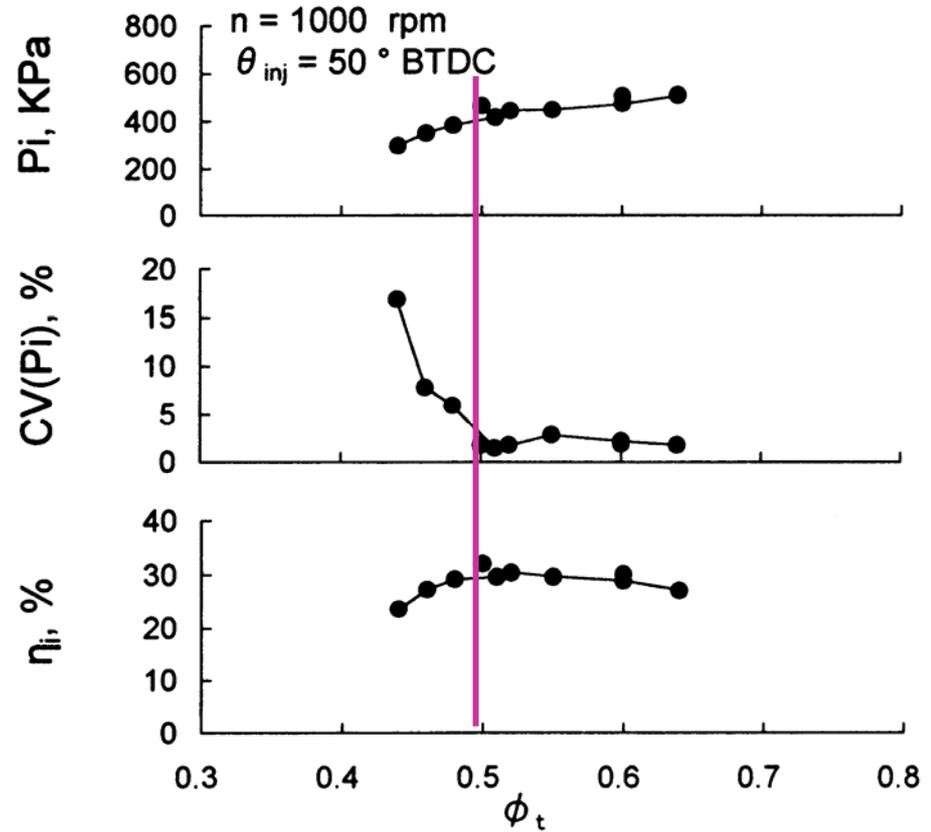
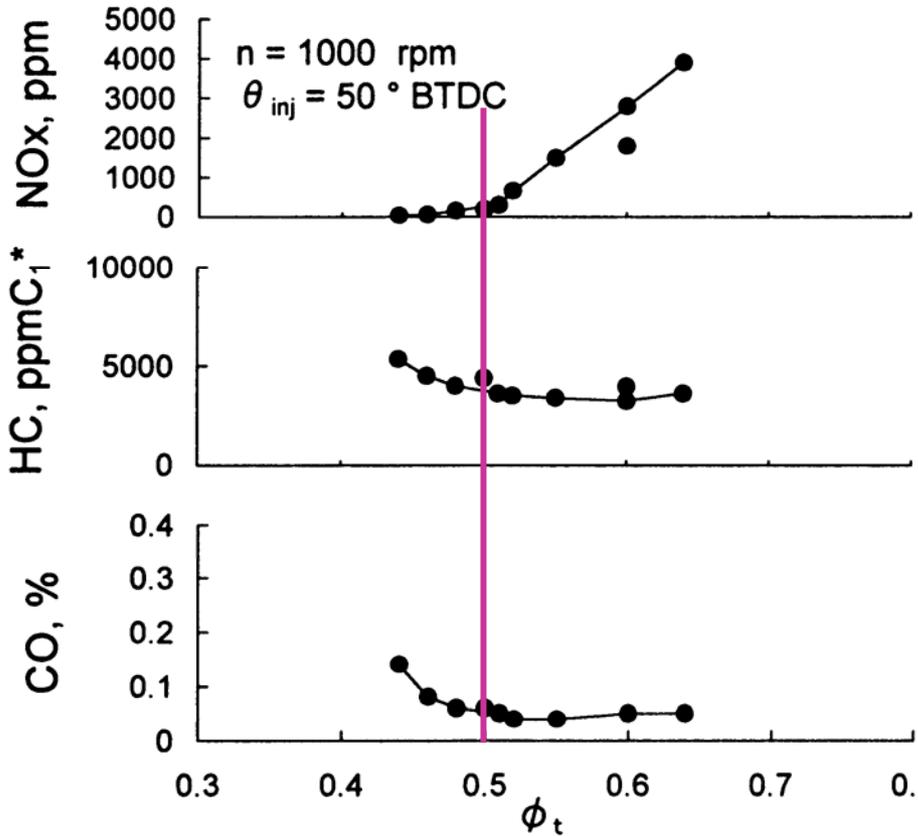


Increase in load

- > {
- increase in  $P_{\max}$  and  $(dQ/d\theta)_{\max}$  and advance in the timing of  $P_{\max}$  and  $(dQ/d\theta)_{\max}$
  - decrease in effective work

$\theta_{inj} = 50 \text{ deg. BTDC}$   
 $(m_{go} = 4 \text{ mg/cycle}, \alpha = 0 \%)$

Pressure and ROHR with increasing load w/o N<sub>2</sub>-dilution



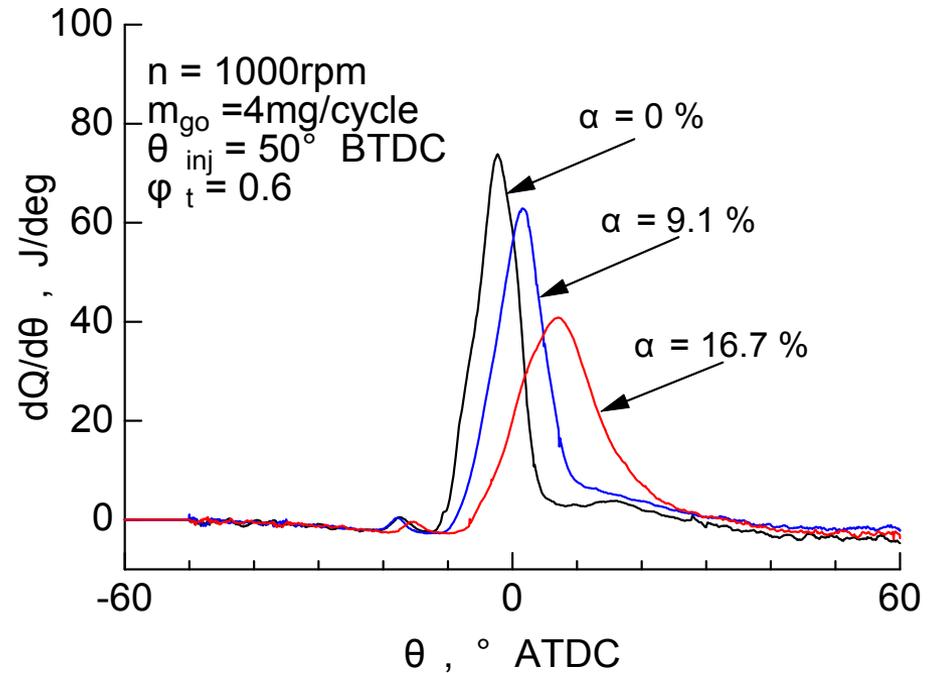
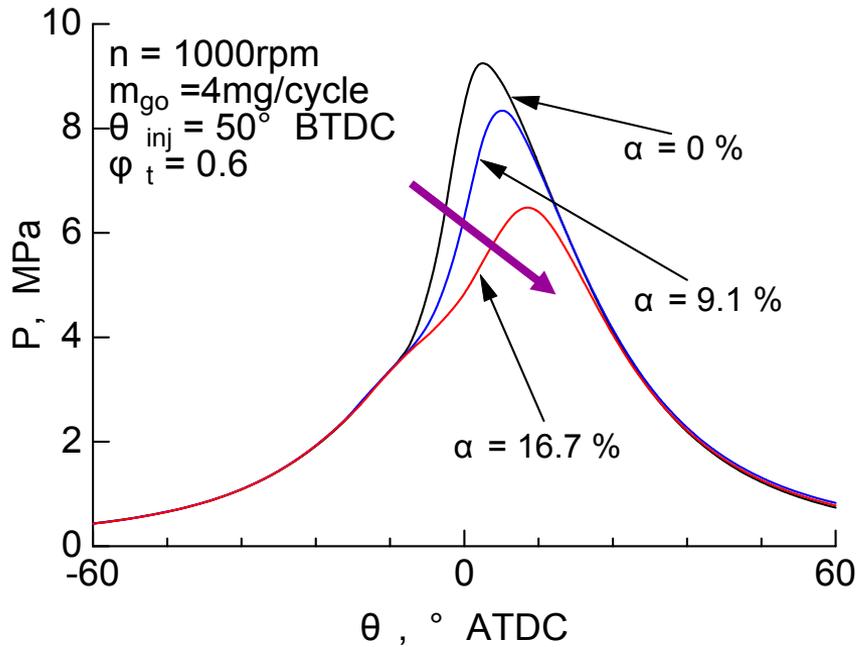
Smoke=0

In  $\phi_t < 0.5$ , combustion is incomplete and bad.

In  $\phi_t > 0.5$ , NOx increases while HC and CO are lower, and combustion becomes stable.

$$m_{go} = 4 \text{ mg/cycle}$$

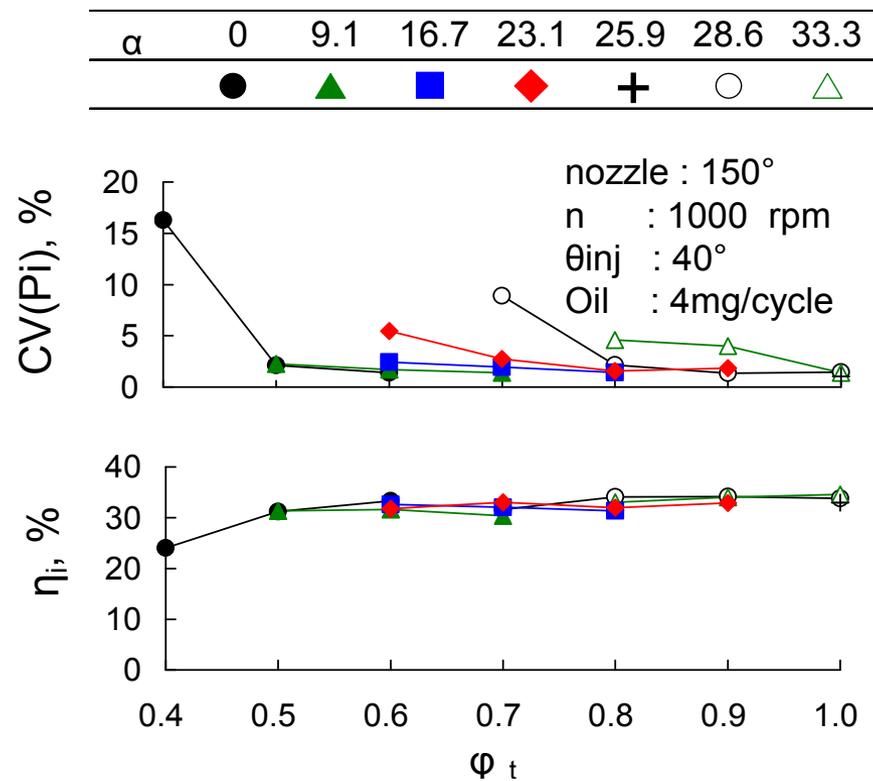
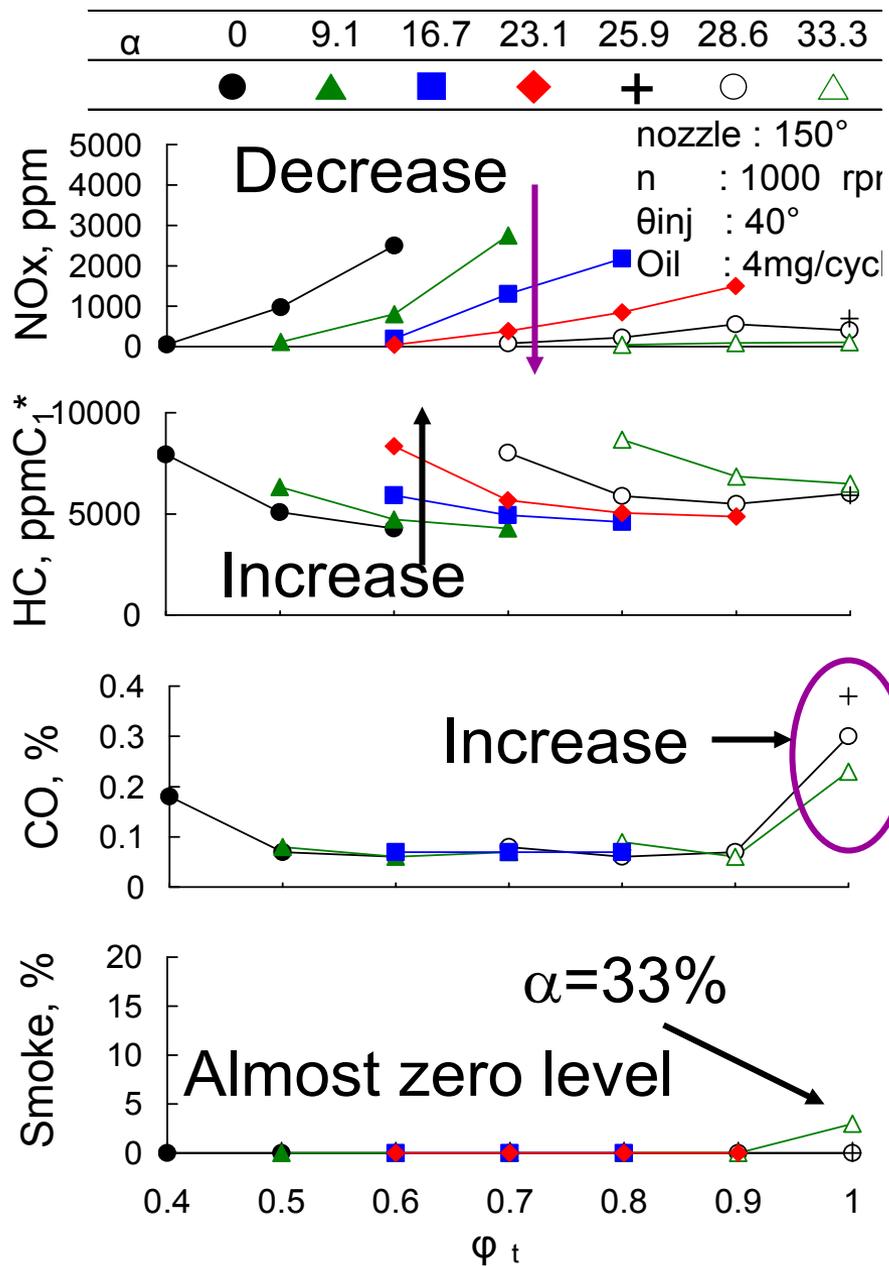
Exhaust emissions and thermal efficiency w/o N<sub>2</sub>-dilution



$N_2$  dilution ratio,  $\alpha=0, 9.1\%, 16.7\%$

When dilution ratio becomes larger,  
the combustion becomes milder.

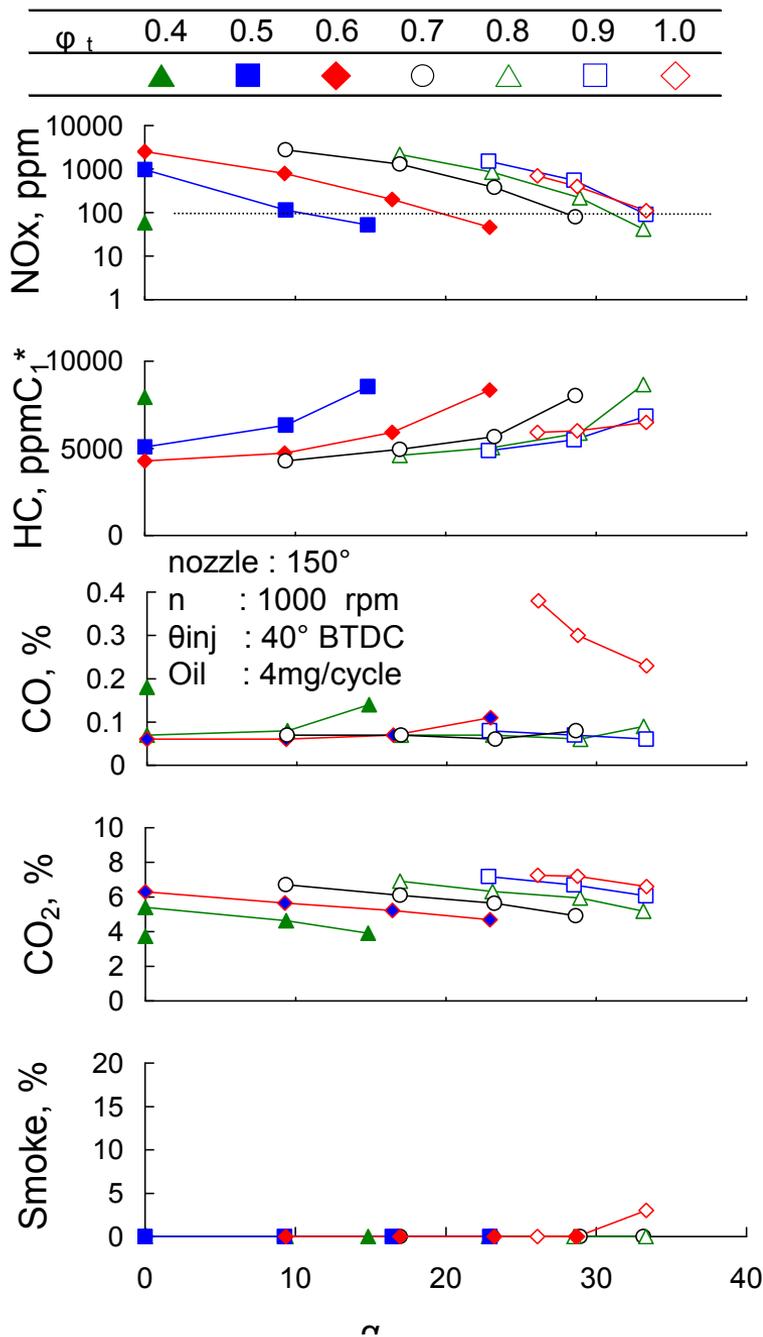
Pressure and ROHR



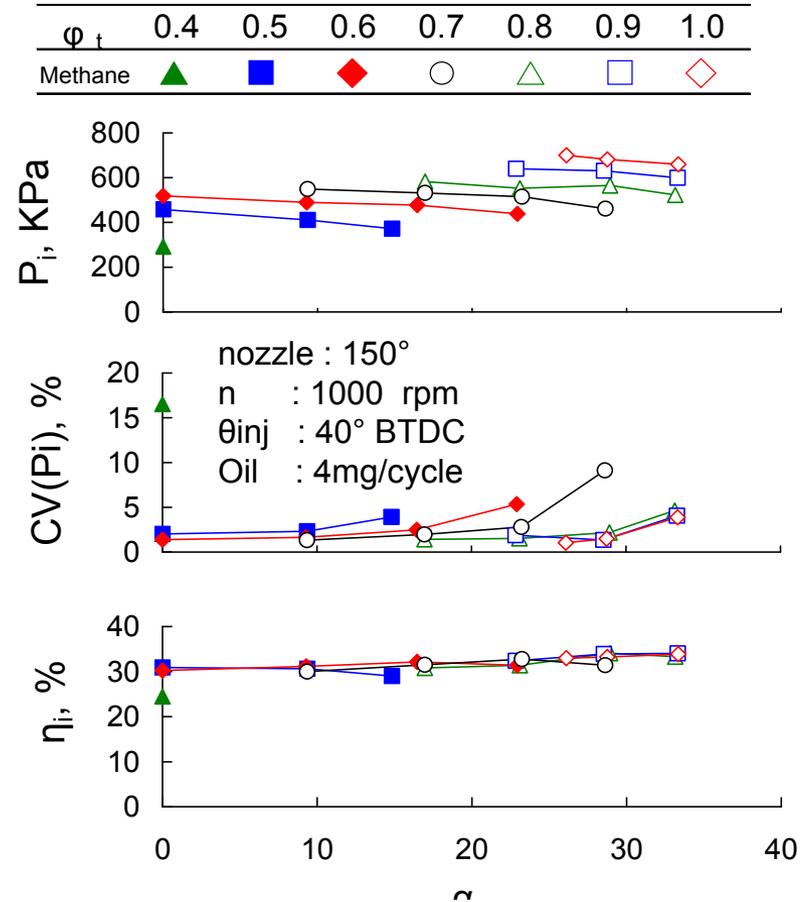
Ratio of N<sub>2</sub>-dilution was changed according to equivalence ratio.

$\theta_{inj}=40^\circ$  BTDC  
(early injection)

Exhaust emissions, thermal efficiency and CV(Pi) with N<sub>2</sub>-dilution



The same data are used.  
 Abscissa: Ratio of N<sub>2</sub> dilution  
 (← Equivalence ratio)  
 NO<sub>x</sub> : log scale

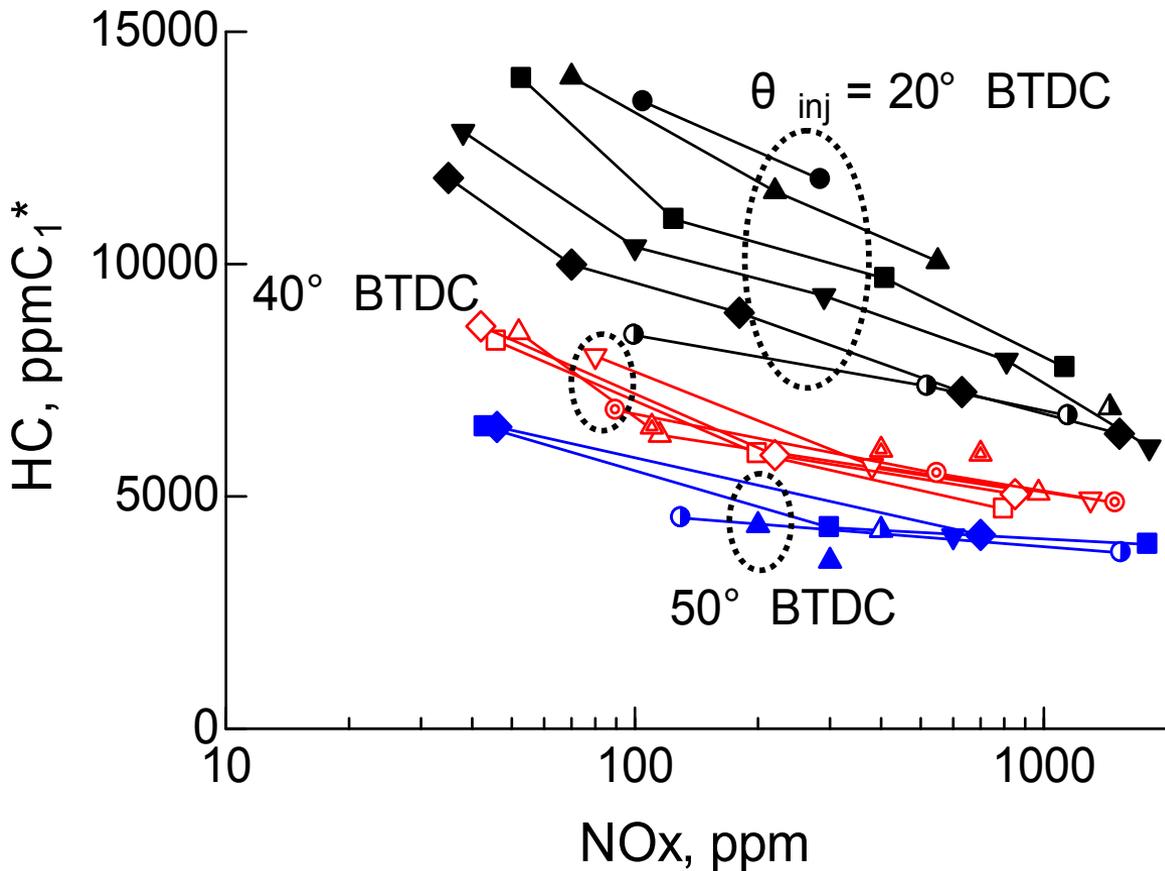


Exhaust emissions with N<sub>2</sub>-dilution

$\theta_{inj} \backslash \varphi_t$	0.4	0.5	0.6	0.7	0.8	0.9	1.0
20 (° BTDC)	●	▲	■	▼	◆	◐	▲
40		△	□	▽	◇	⊙	△
50		▲	■	▼	◆	◐	▲

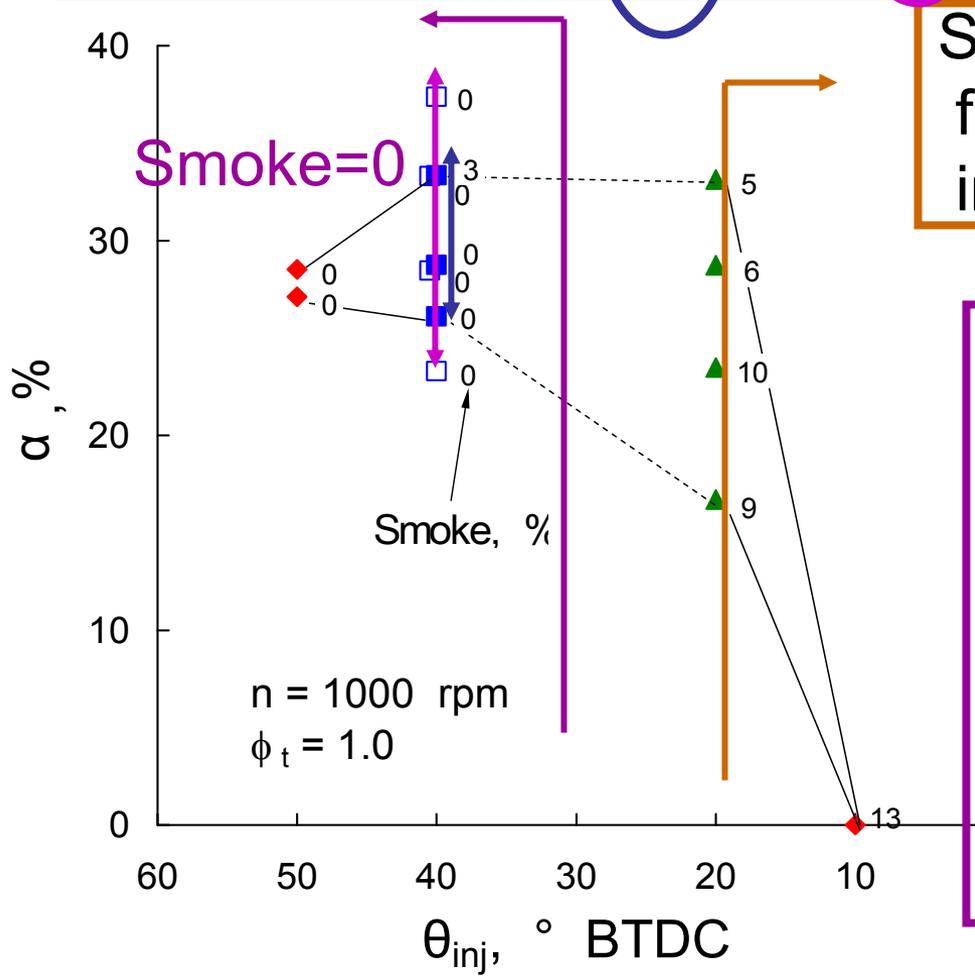
Trade off of  
HC and NOx

Early injection  
(20 → 40 → 50  
deg. BTDC)  
- Lower HC



Relation between HC and NOx

$\theta_{inj}$ ( $^{\circ}$ BTDC)	10	20	40	50	40
$m_{go}$ (4mg/cycle)	4	4	4	4	8
	●	▲	■	◆	□



Smoke could be seen due to fuel-rich region in normal injection .

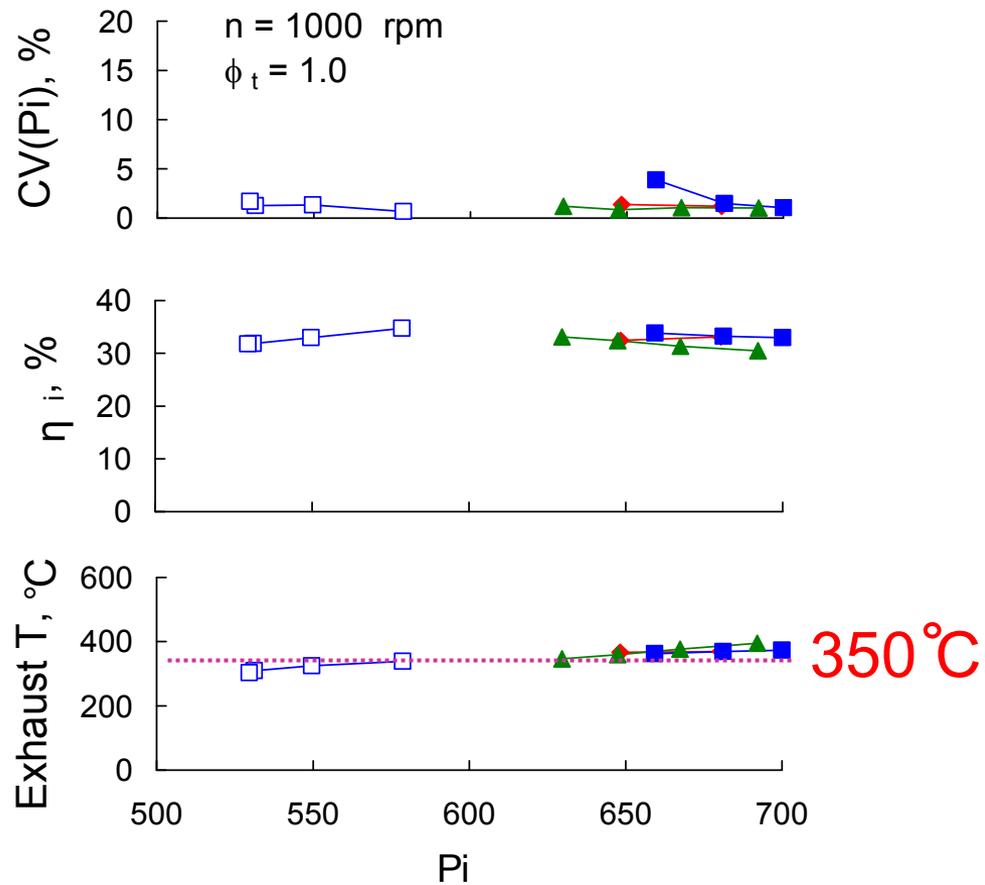
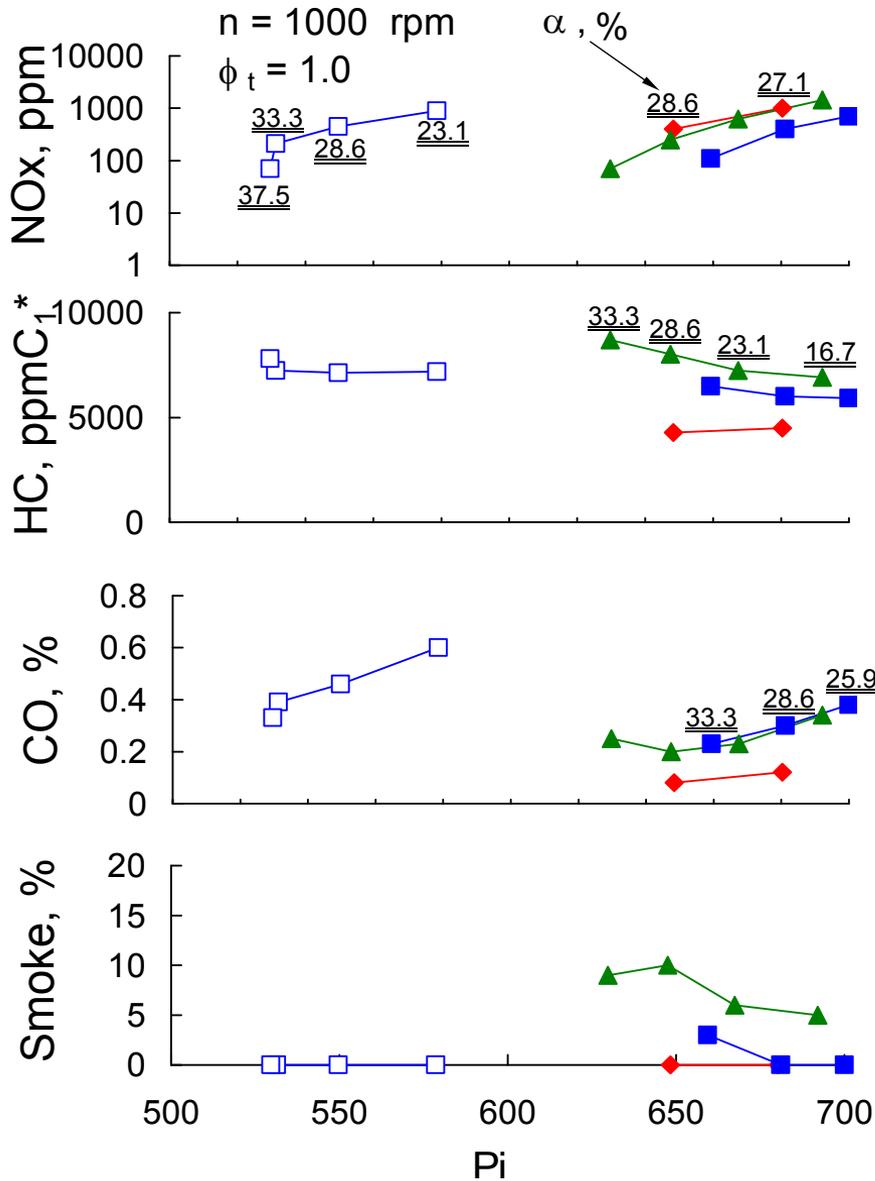
In early injection, smoke level is almost zero and operating range becomes narrow.

When diesel fuel increases, the operating range in  $\phi_t=1.0$  becomes wider.

## Operating range of stoichiometric conditions

$\theta_{inj}$ ( $^{\circ}$ BTDC)	10	20	40	50	40
$m_{go}$ (4mg/cycle)	4	4	4	4	8
	●	▲	■	◆	□

$\theta_{inj}$ ( $^{\circ}$ BTDC)	10	20	40	50	40
$m_{go}$ (4mg/cycle)	4	4	4	4	8
	●	▲	■	◆	□



**Stoichiometric conditions**

(1) When the injection timing of diesel fuel is advanced, the range of equivalence ratio for the engine operation becomes narrow.

However, the engine can operate even in stoichiometric mixture owing to N<sub>2</sub>-dilution.

Under the condition of stoichiometric mixture, smoke can be seen when the injection timing is 20 degrees BTDC though smoke is not seen when the injection timing is 40 and 50 degrees BTDC.

This is because there is no rich region of fuel due to the diffusion of the diesel fuel in the early injection.

- (2) The peak of the rate of heat release is retarded in the early injection timing. The exhaust emissions of NO<sub>x</sub> are very low and HC and CO are almost the same while thermal efficiency increases slightly.
- (3) In the early injection timing without N<sub>2</sub>-dilution, when the equivalence ratio increases, the effective work decreases because the maximum value of the heat release is advanced and thermal efficiency decreases.
- (4) The value of the hydrocarbons in the early injection is smaller than those in the normal injection timing though the absolute value seems to be large.

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## Conclusions (2)

### 3) Recent research and tools

#### a) Spectroscopic analysis of burned gas

Small fiber optics is used for local spectroscopic analysis. OH, CH and C<sub>2</sub> radicals are detected and combustion characteristics such as heat release rate, flame developing speed.

#### b) Local gas temperature measurement using interferometry system

Interferometry technique is applied to measure temperature history of the gas with a small sensor that is developed in my laboratory. The degree of homogeneity of the temperature in the cylinder can be obtained.