

Thirty-Second Task Leaders Meeting
International Energy Agency Implementing Agreement
on Energy Conservation and Emissions Reduction in Combustion
Nara Royal Hotel, Nara, Japan, July 25-29

1.6A.06: Okayama University, Japan

Prof. Eiji Tomita

Dual fuel: Premixed gaseous fuel and diesel direct injection

Effect of component of biomass-based gaseous fuels
on combustion in a super-charged gas engine with
micro-pilot injection



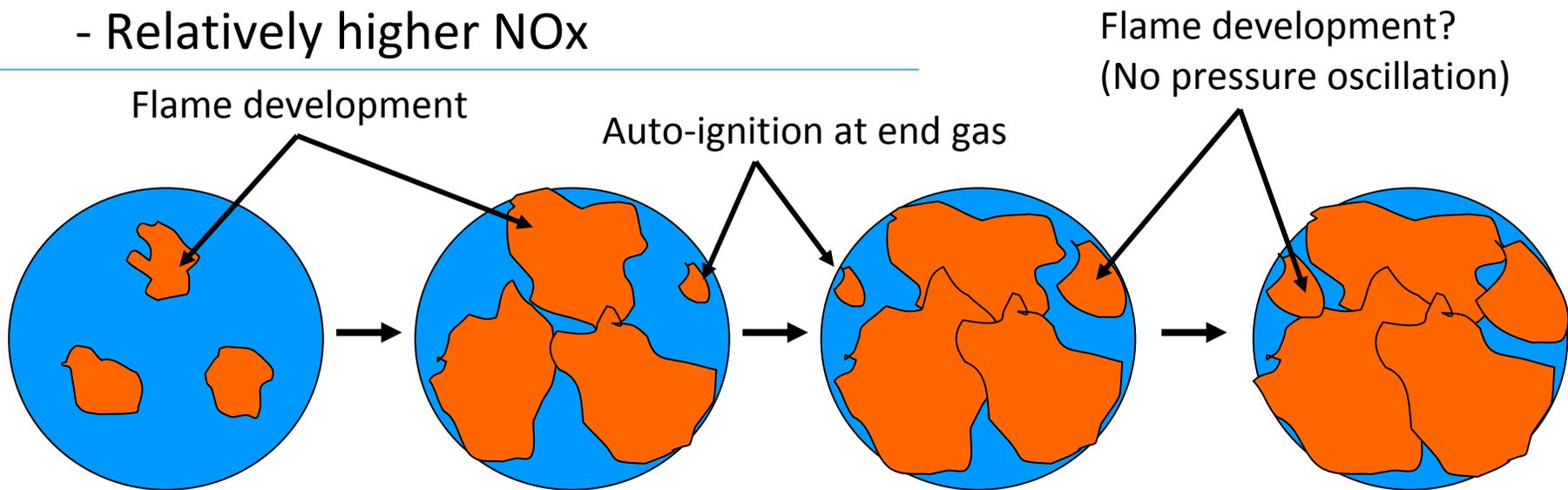
Eiji Tomita,
Kawahara Nobuyuki,
Murari Mohon Roy
(Okayama University)

Flame development → auto-ignition without knock
→ other flame developments
or mild auto-ignition

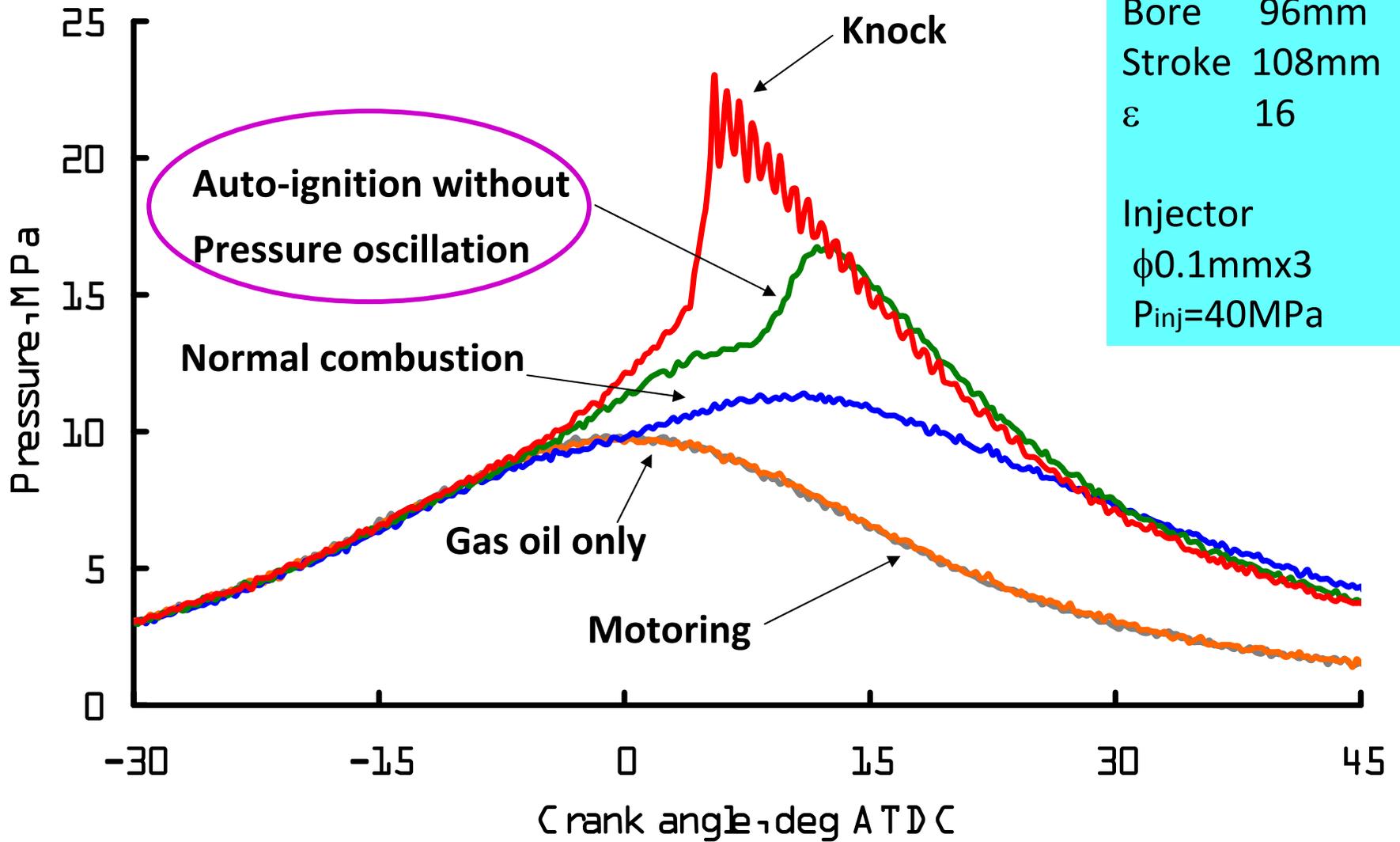
Engine: Lean burn gas engine ignited with diesel fuel (Gas oil)

Features

- Higher thermal efficiency
- Lower HC
- Relatively higher NO_x



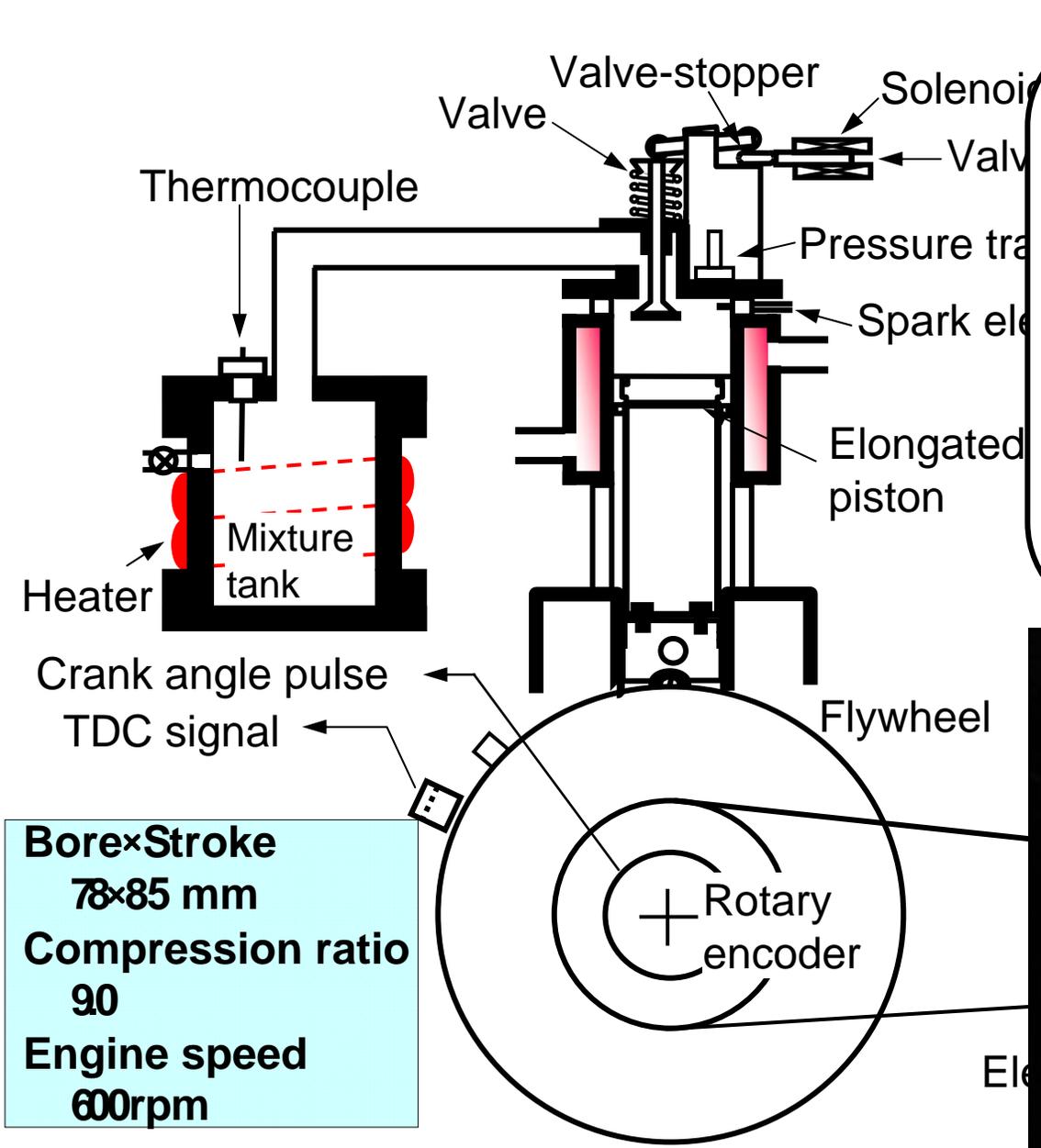
Motivation



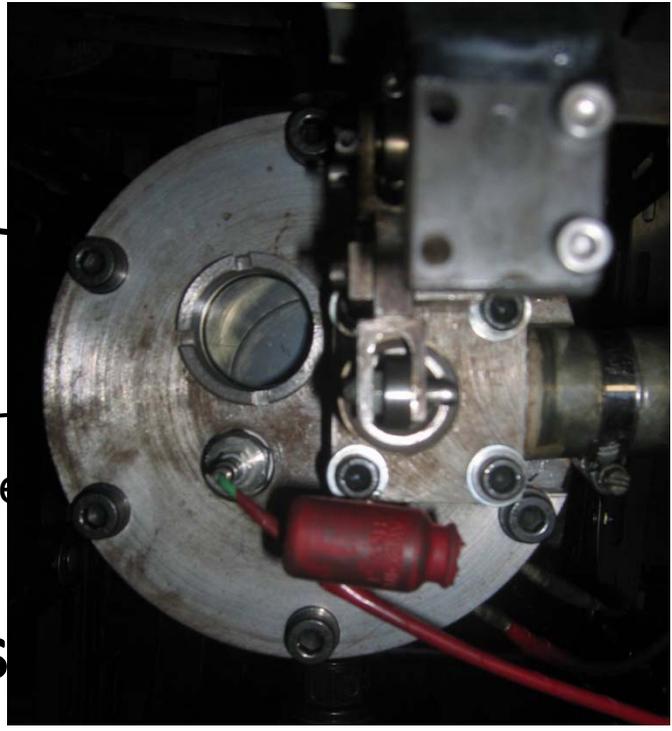
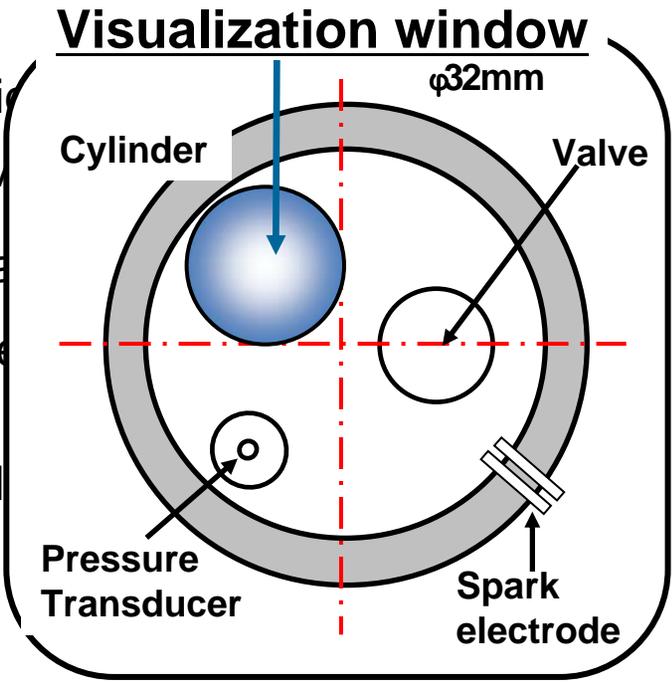
Bore 96mm
 Stroke 108mm
 ϵ 16
 Injector
 ϕ 0.1mmx3
 P_{inj} =40MPa

$n=1000\text{rpm}$, Natural gas + diesel fuel $\phi_t=0.6$, $m_{go}=2.0\text{mg/cycle}$, $P_{in}=200\text{kPa}$

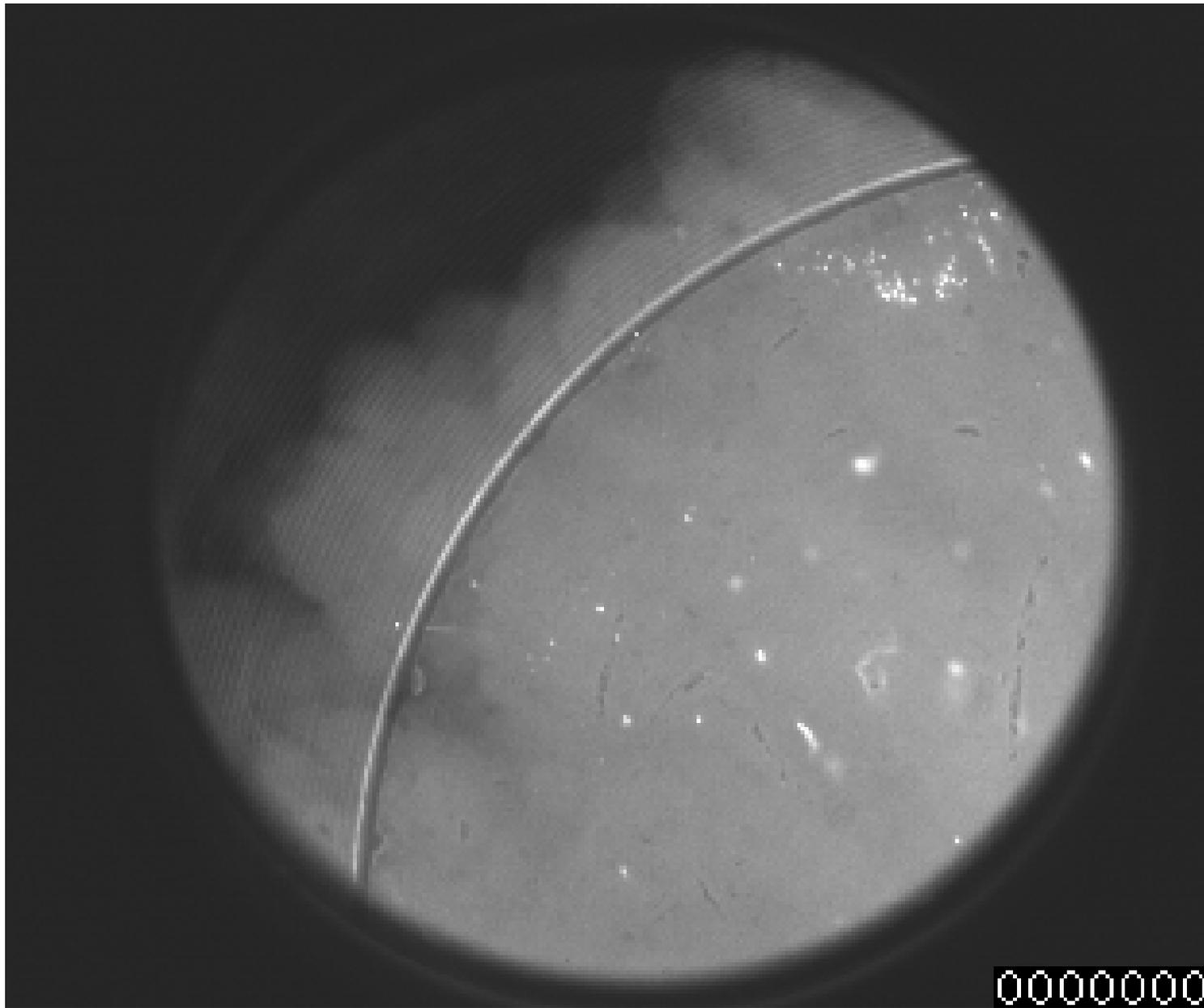
Natural gas engine ignited with pilot diesel fuel



Bore×Stroke
78×85 mm
Compression ratio
90
Engine speed
600rpm

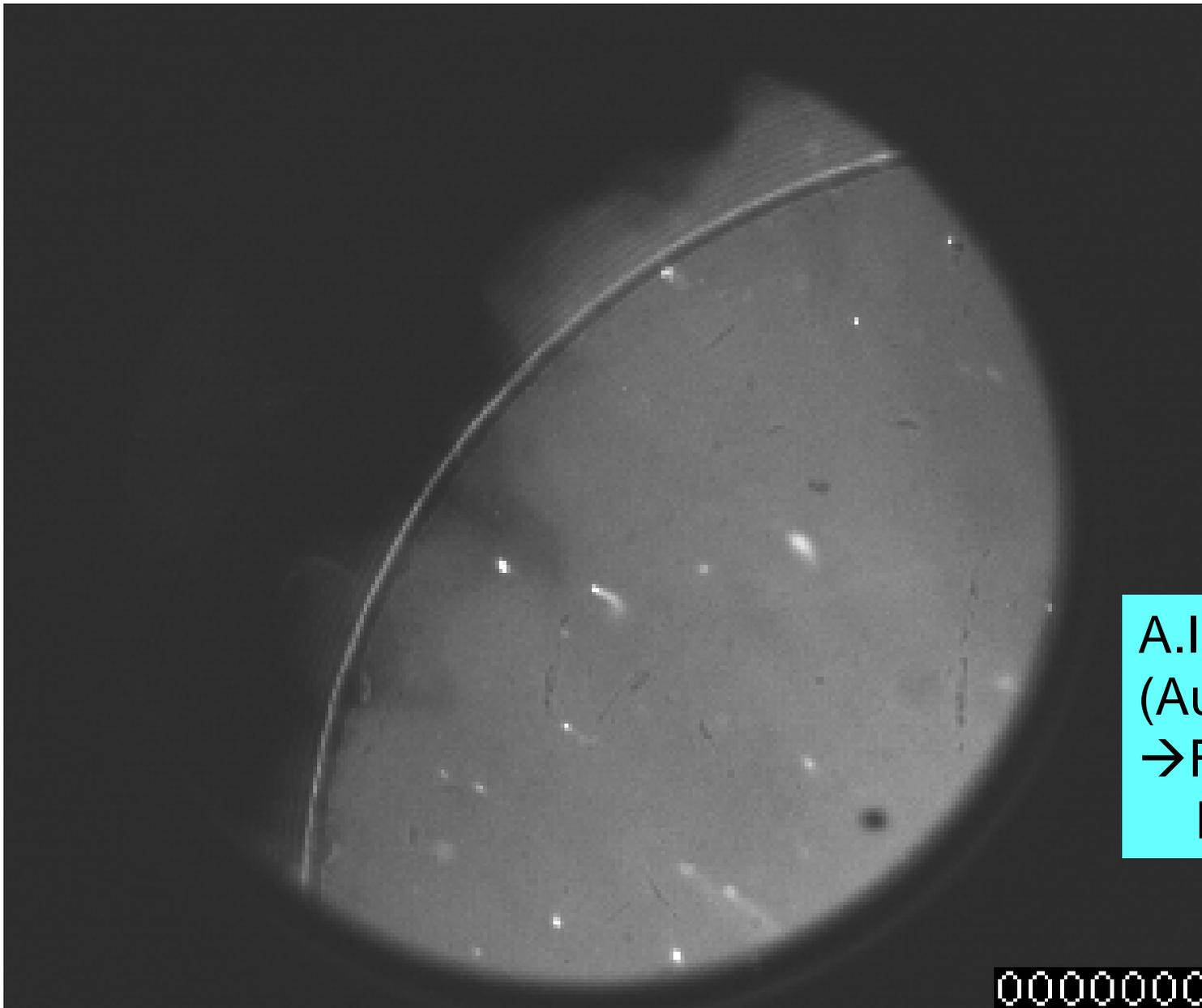


Experimental s



Knock

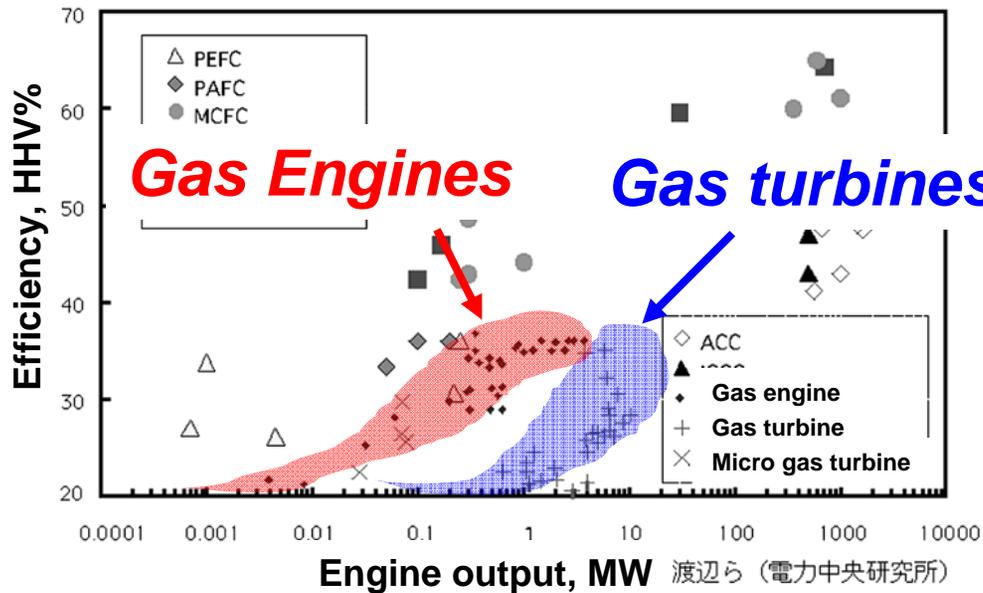
Combustion near end gas region with a high-speed video camera



A.I. → F.P.
(Auto-ignition
→ Flame
Propagation)

Combustion near end gas region with a high-speed video camera

Power generation



Reference

http://www.iae.or.jp/publish/kihou/29-1/03_7.html

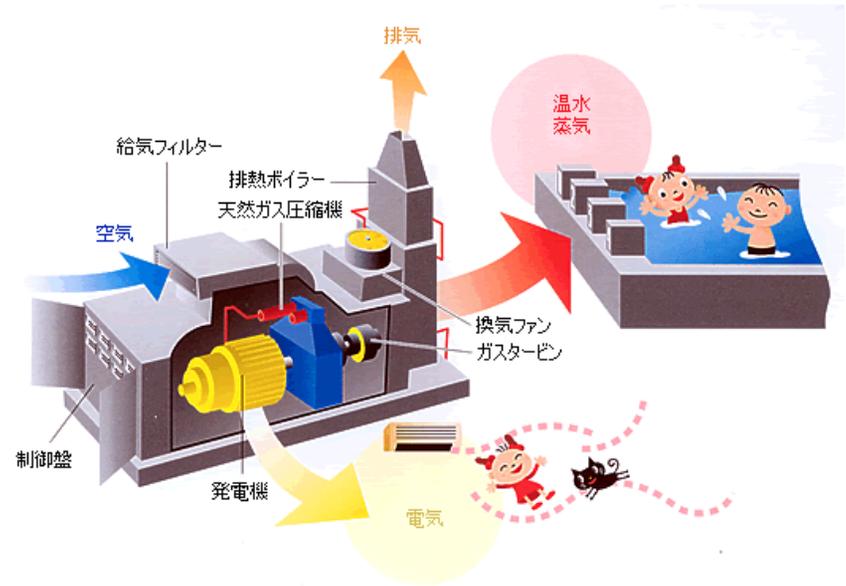
Gas Engines

Gaseous fuel



High octane number

Ignition systems



Dual-fuel gas engine

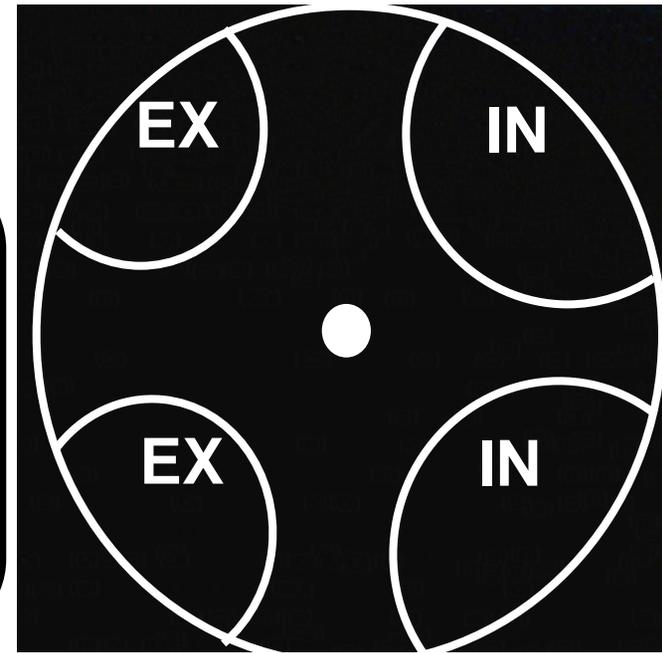
(6 cylinders, 1000kW)

Background

Dual-fuel system

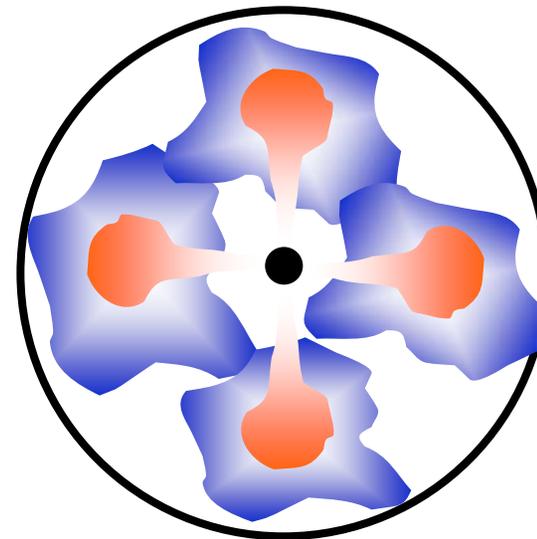
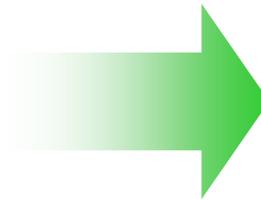
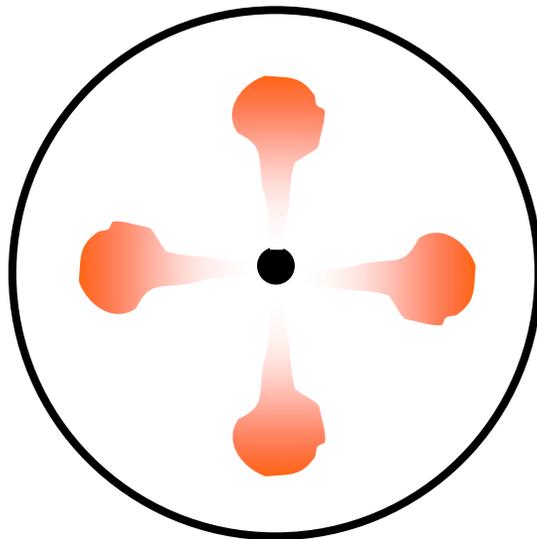
Diesel fuel ; **ignition sources**

- *Multi-point ignition*
- *Easy control of ignition energy*
- *High power and thermal efficiency*

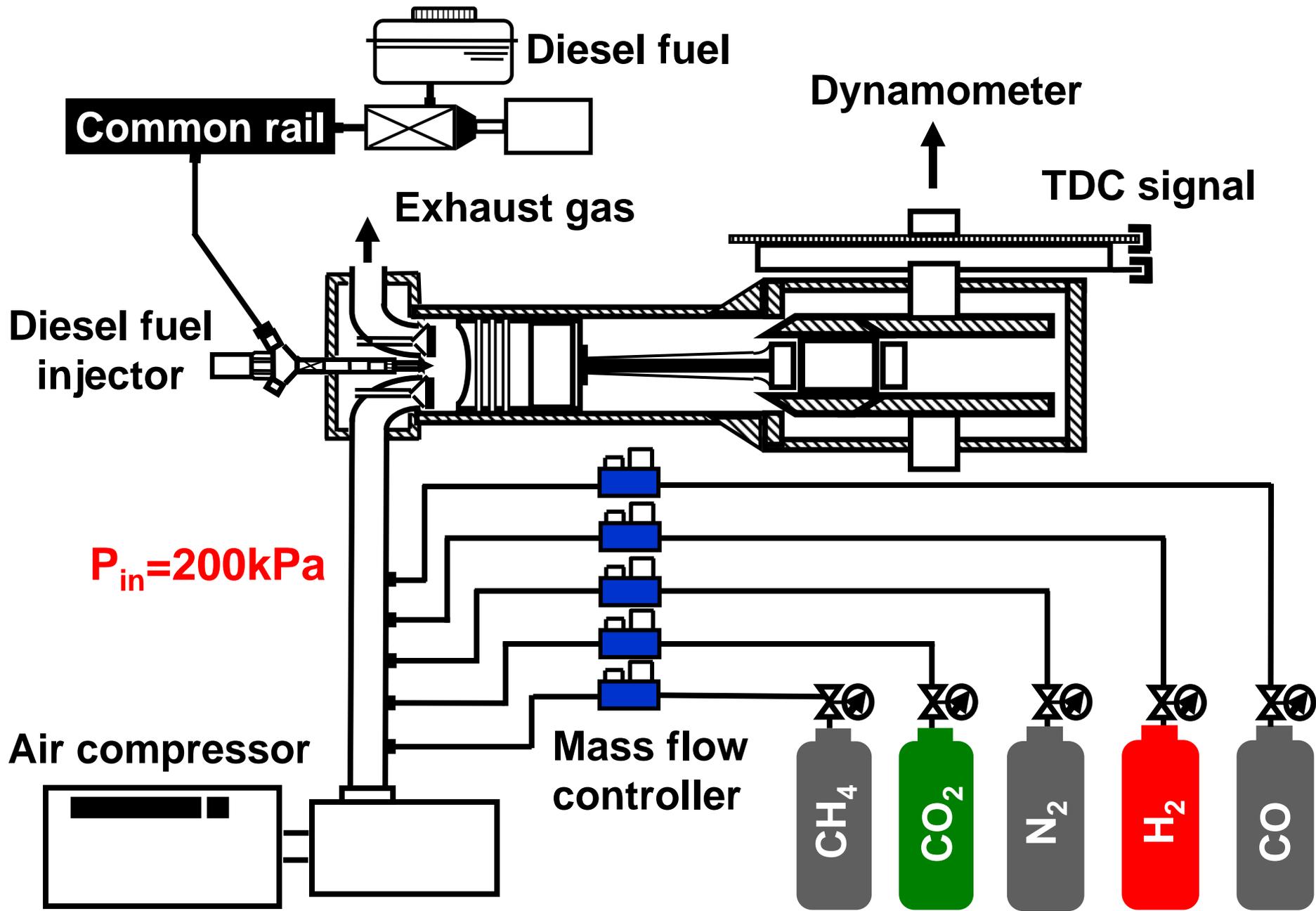


Auto-ignition of diesel fuel

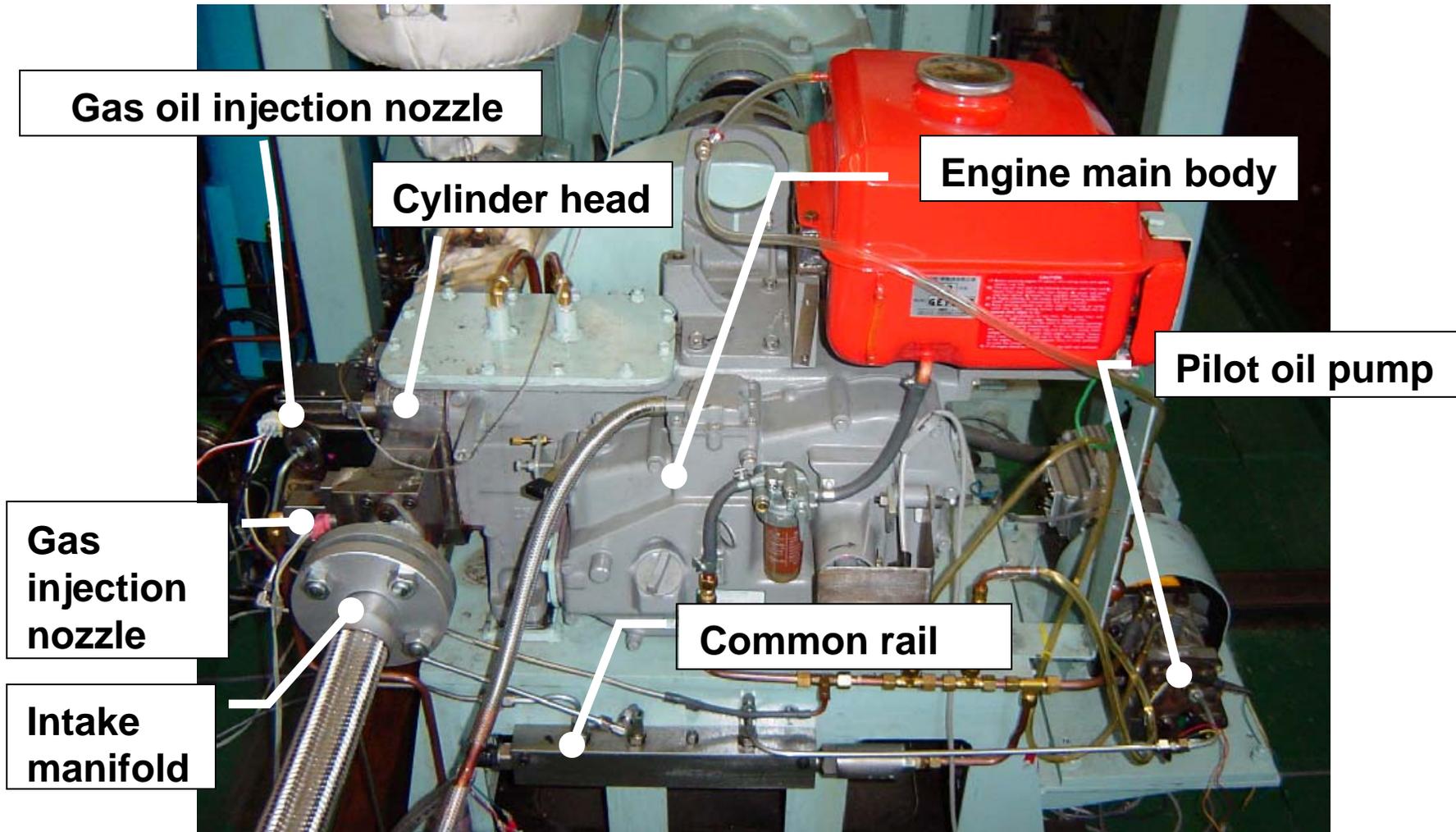
Flame development of gaseous fuel



Dual - fuel system



Experimental apparatus

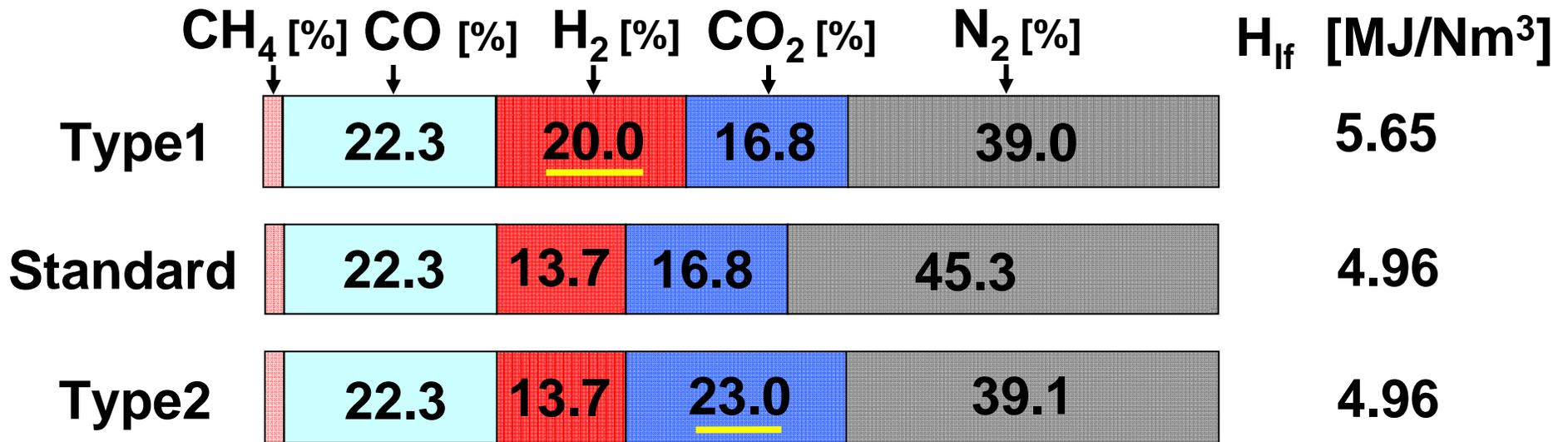


Bore×Stroke 96×108 mm (782 cc)

Compression ratio 16.0

Engine speed 1000 rpm

Intake pressure 200 kPa



1.9

- Standard : Biomass gas made of wood tips
- Type1 : H₂-enriched
- Type2 : CO₂-enriched

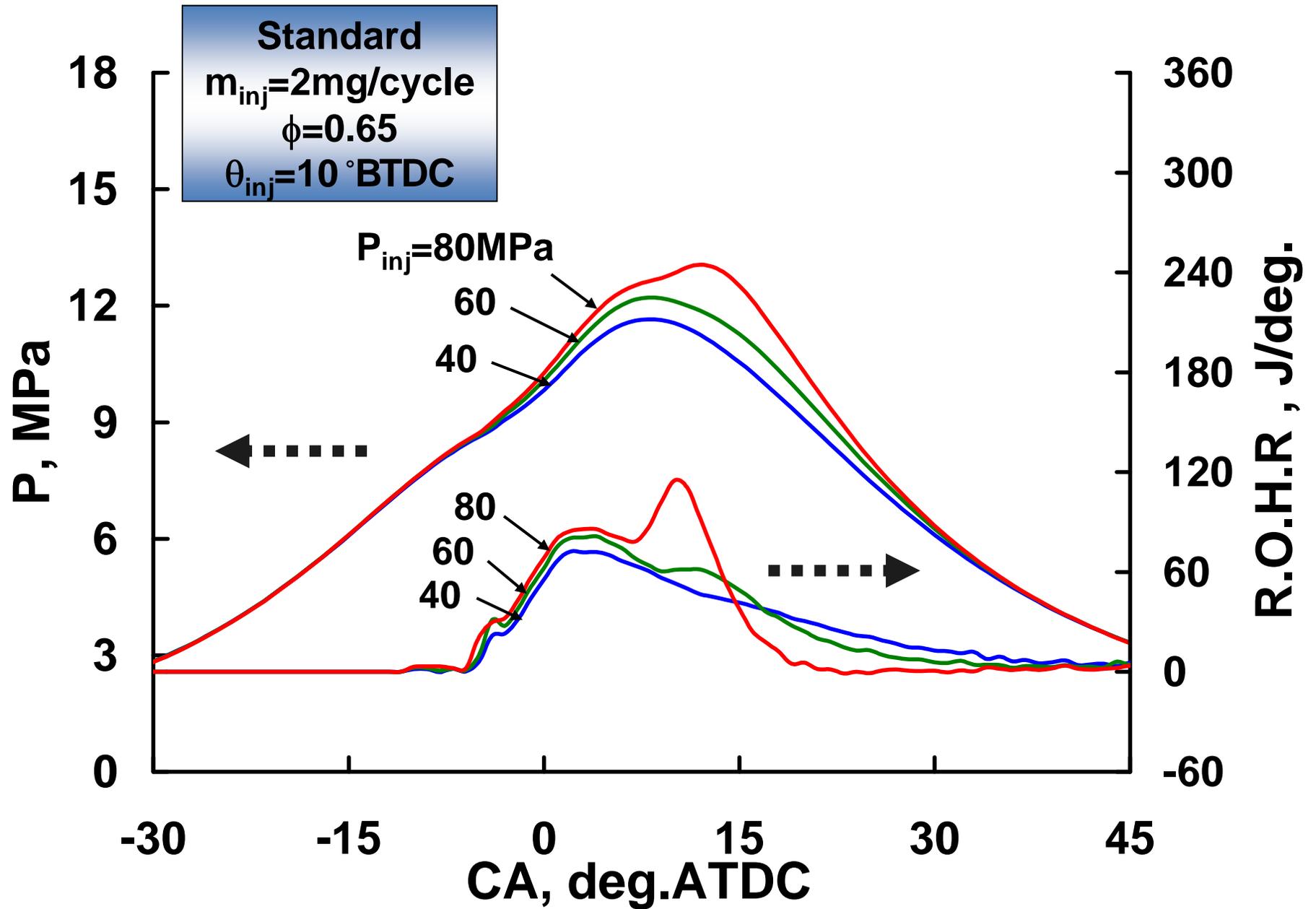
	CH ₄ [%]	C ₂ H ₆ [%]	C ₃ H ₈ [%]	C ₄ H ₁₀ [%]	H _{lf} [MJ/Nm ³]
NG(13A)	88.9	6.8	3.1	1.2	39.2

Gas components

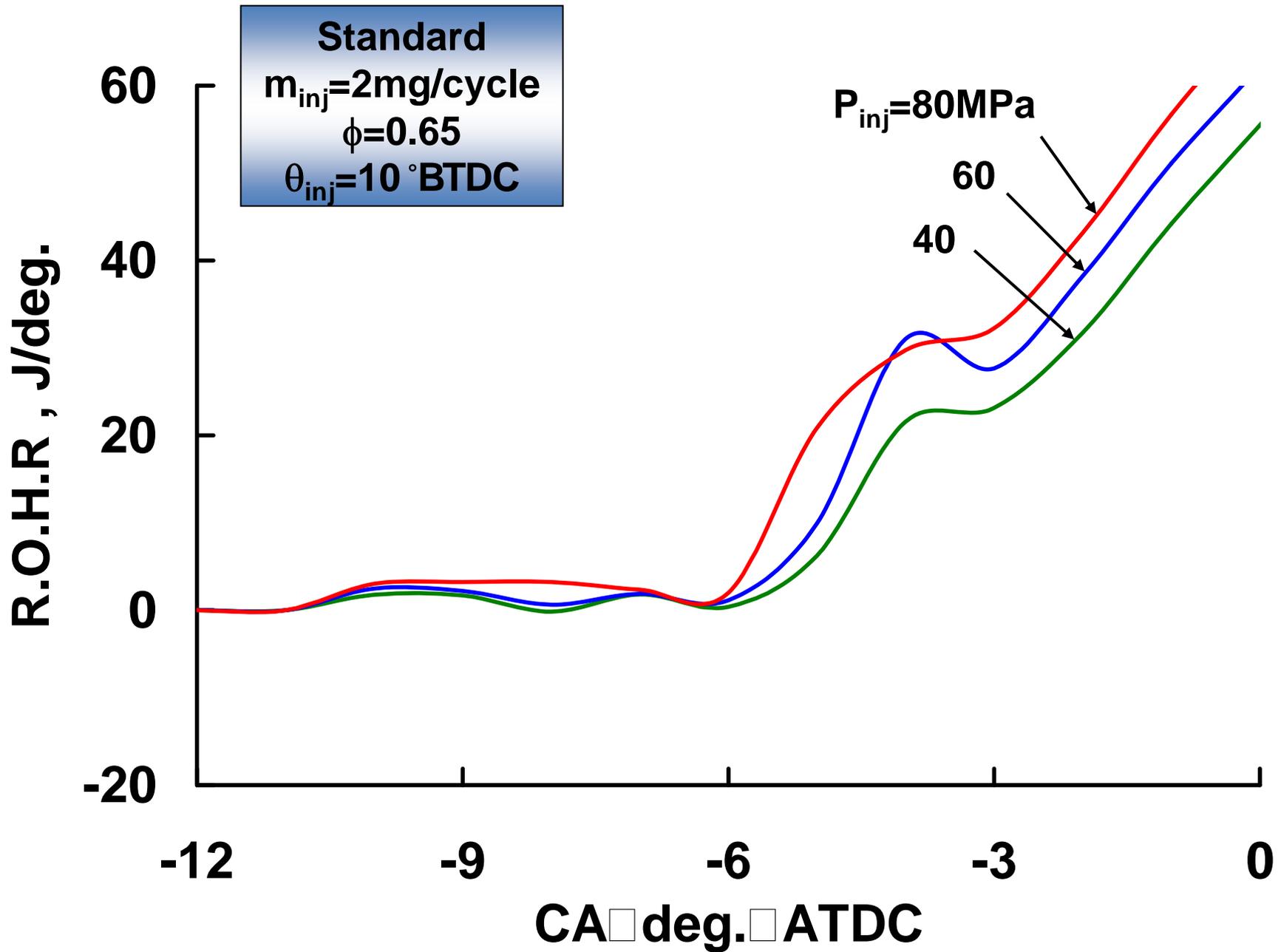
Effects of injection pressure and amount of diesel fuel on combustion and exhaust emissions

Standard

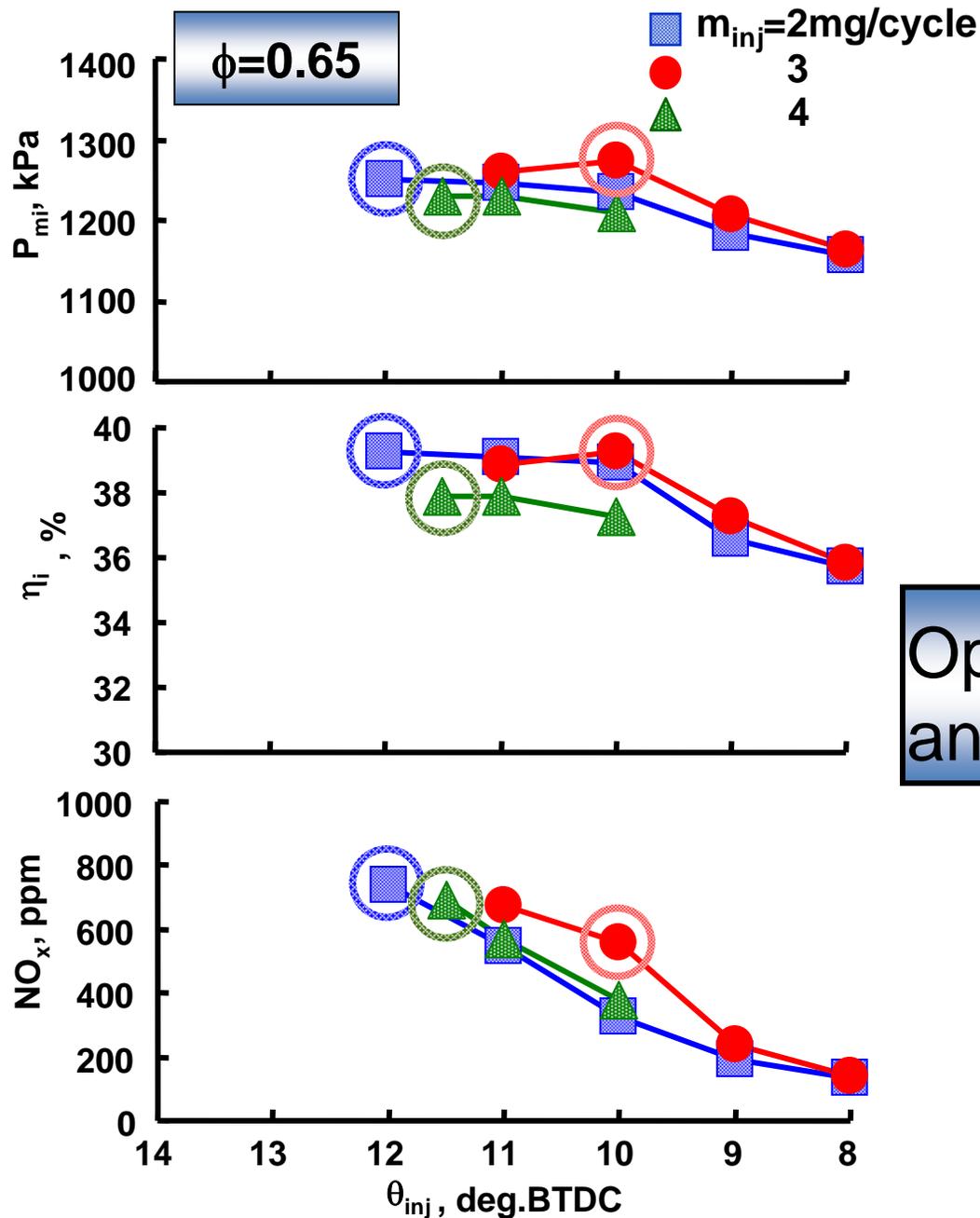
$$\phi_{\square} = 0.65$$



Effect of injection pressure of diesel fuel ($m_{inj}=2\text{mg/cycle}$)



Effect of injection pressure of diesel fuel on ROHR



IMEP

High load

Thermal efficiency

High efficiency

Optimum injection pressure
and amount of diesel fuel

$P_{inj}=80\text{MPa}$

$m_{inj}=3\text{mg/cycle}$

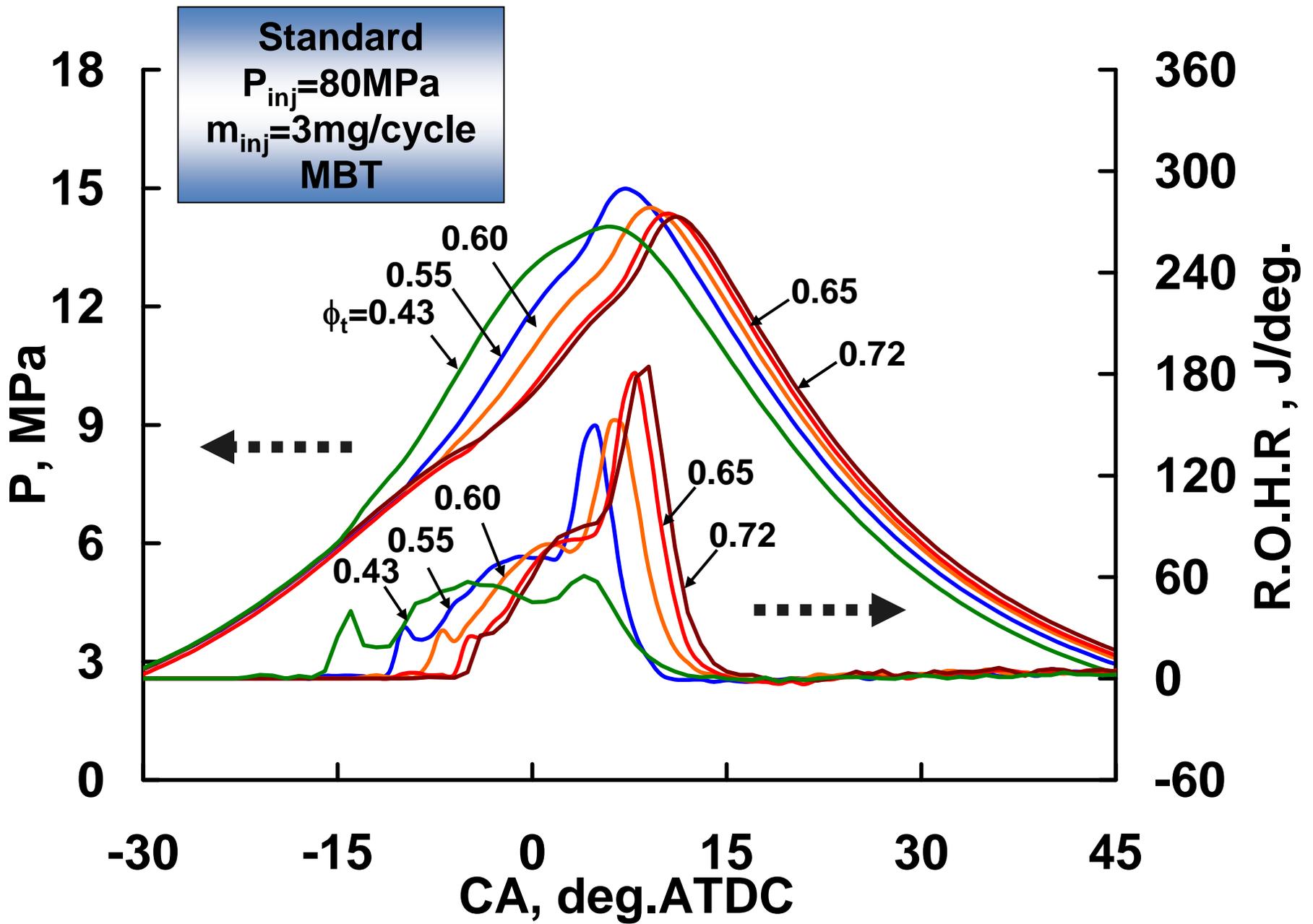
Effect of amount of diesel fuel on combustion ($P_{inj}=80\text{MPa}$)

Effect of equivalence ratio on combustion and exhaust emissions

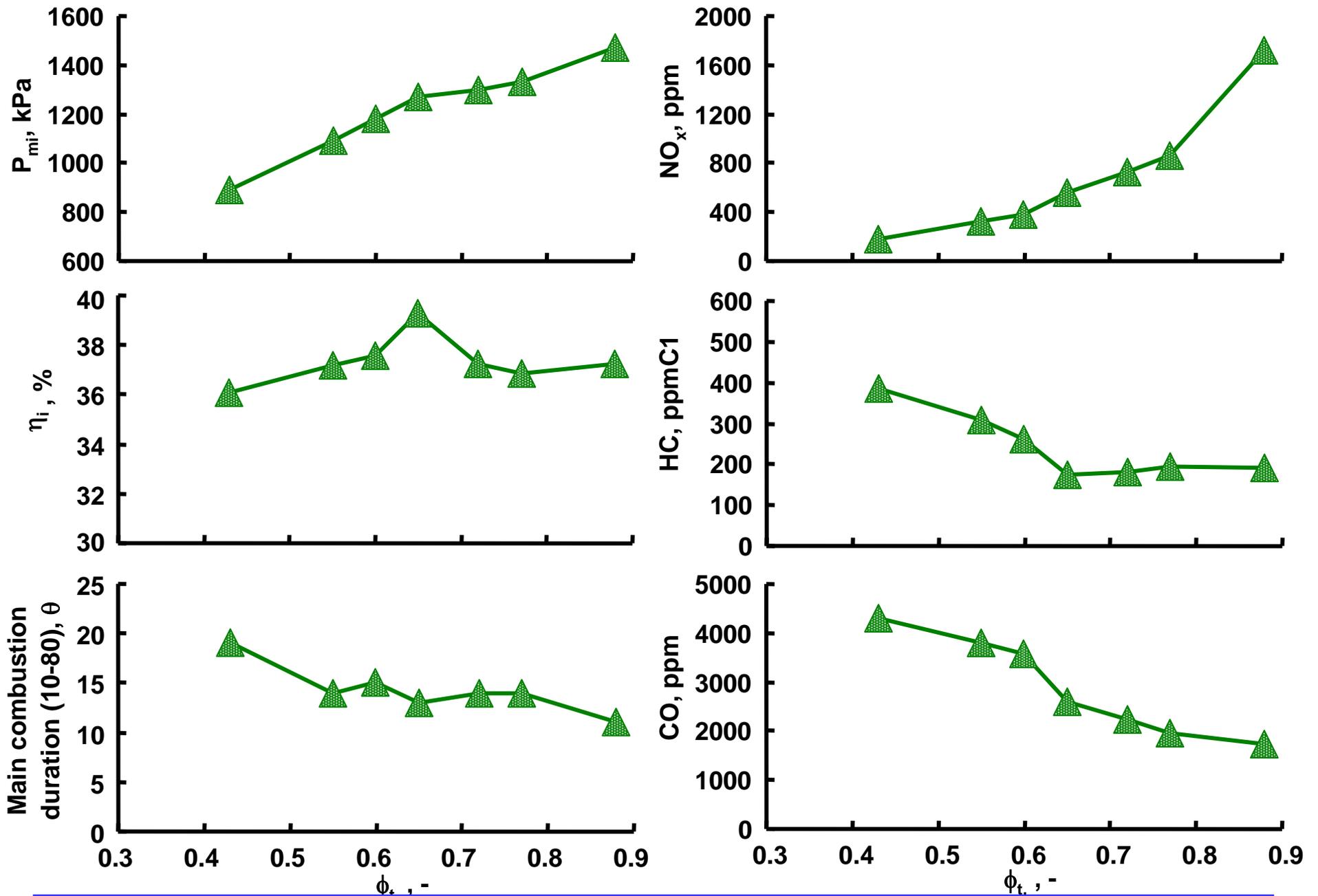
Standard

$$P_{inj} = 80 \text{ MPa}$$

$$m_{inj} = 3 \text{ mg/cycle}$$



Effect of equivalence ratio on pressure history and ROHR



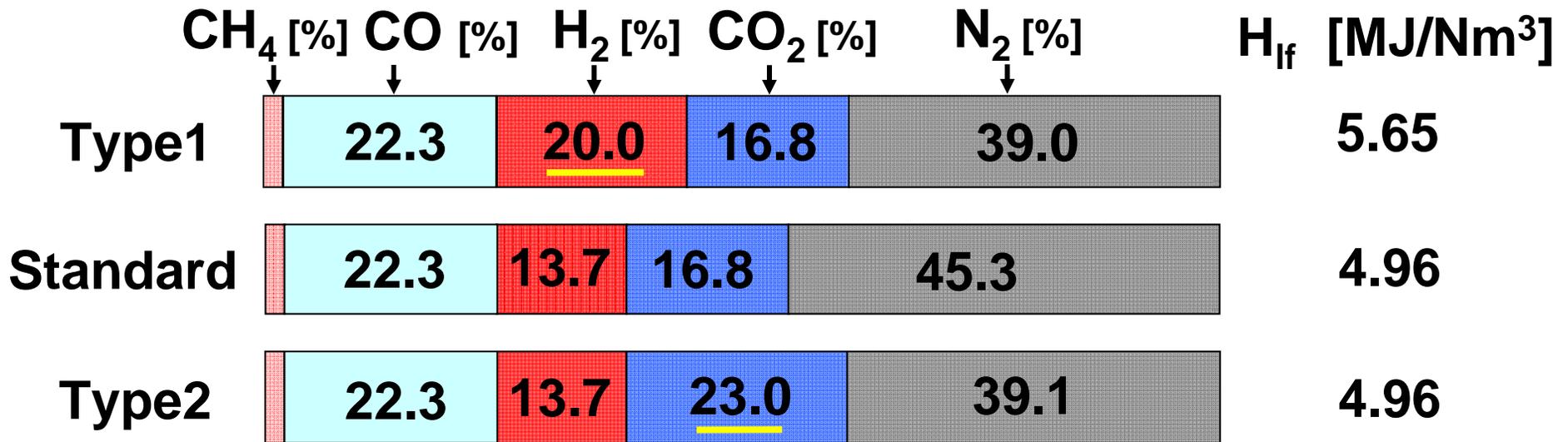
Effect of equivalence ratio on engine performance (Standard)

Effect of equivalence ratio on engine performance and exhaust emissions

$$P_{inj} = 80 \text{MPa}$$

$$m_{inj} = 3 \text{mg/cycle}$$

Standard, **Type1, Type2**



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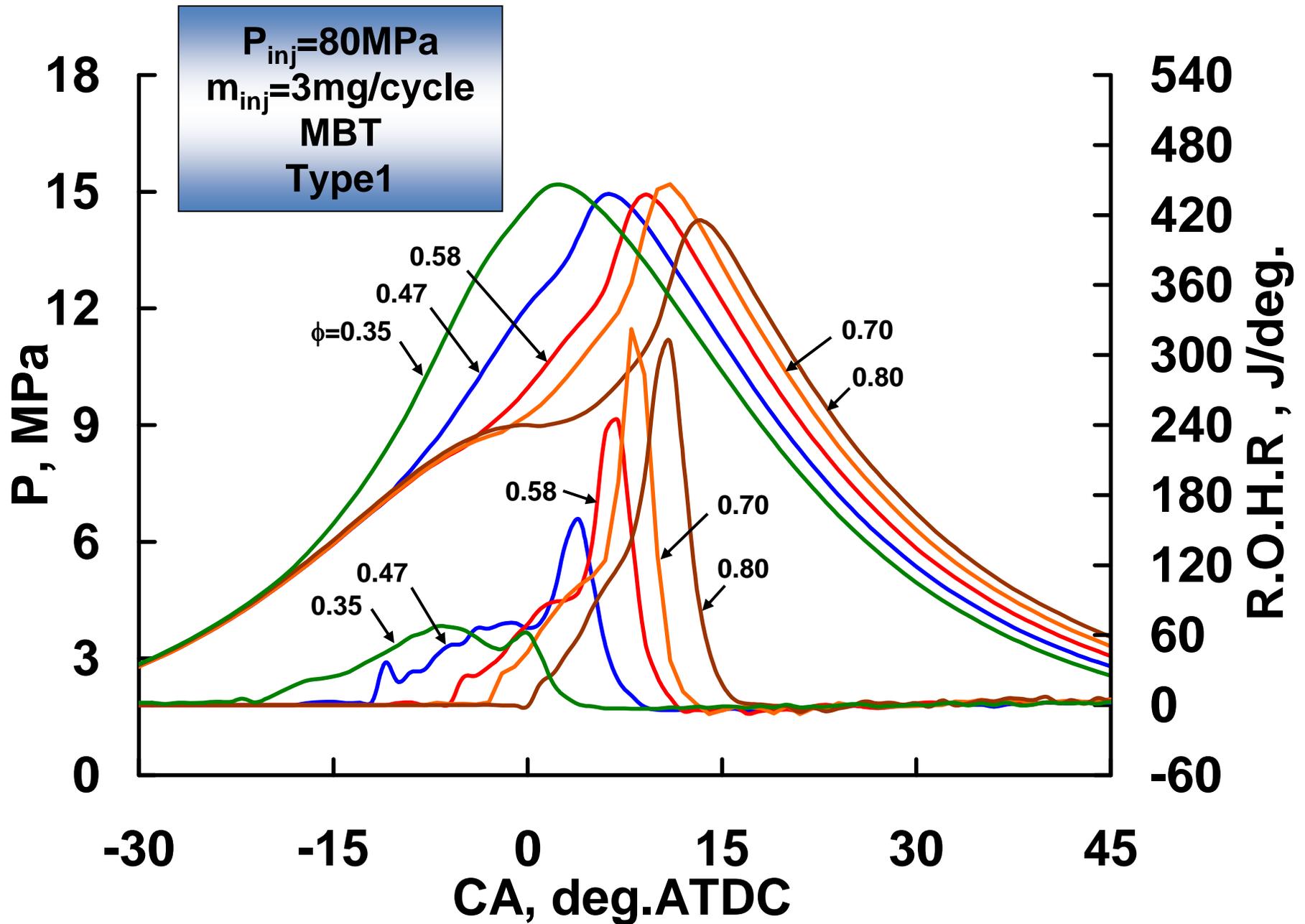
Standard : Biomass gas made of wood tips

Type1: H₂-enriched

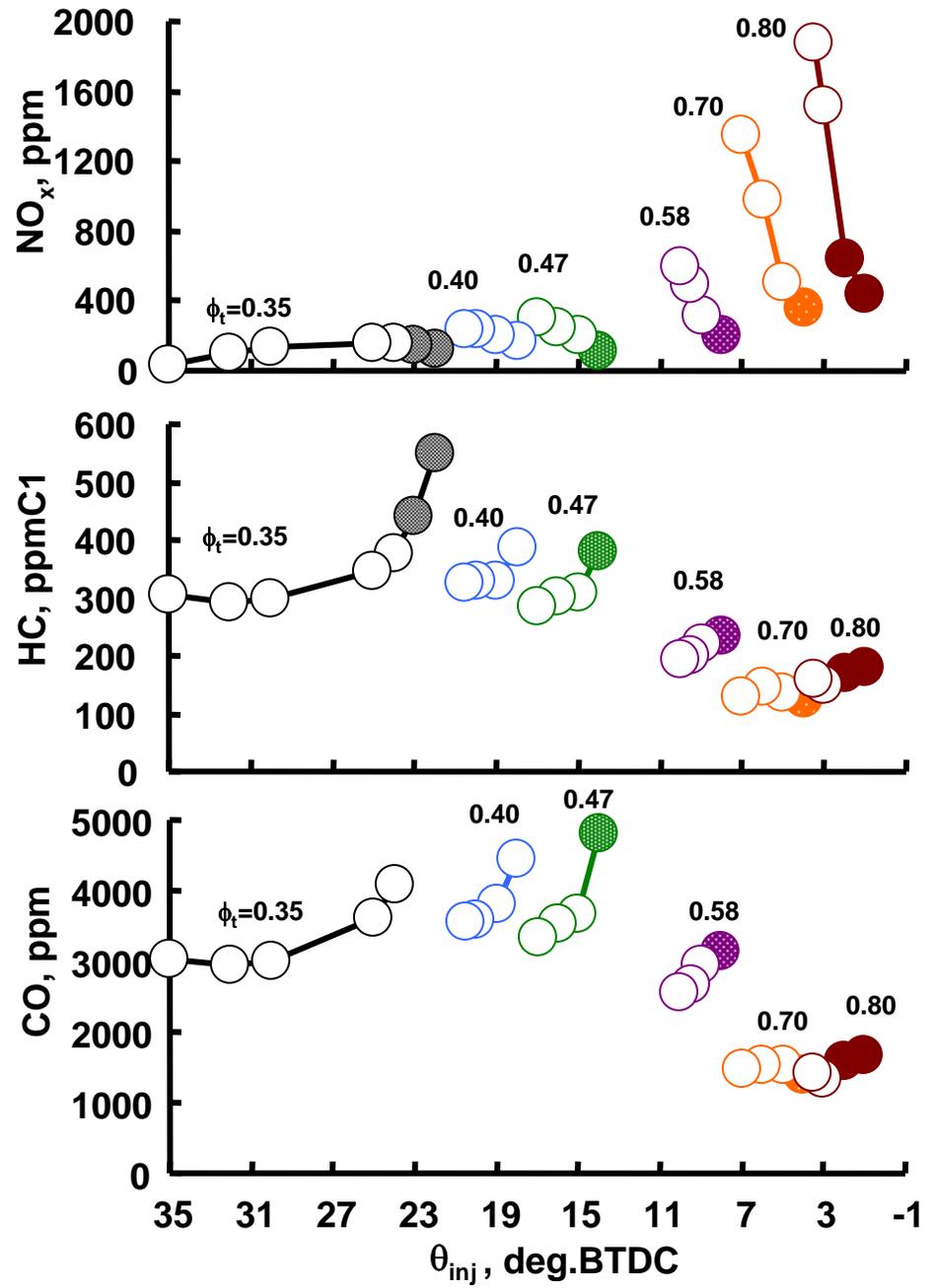
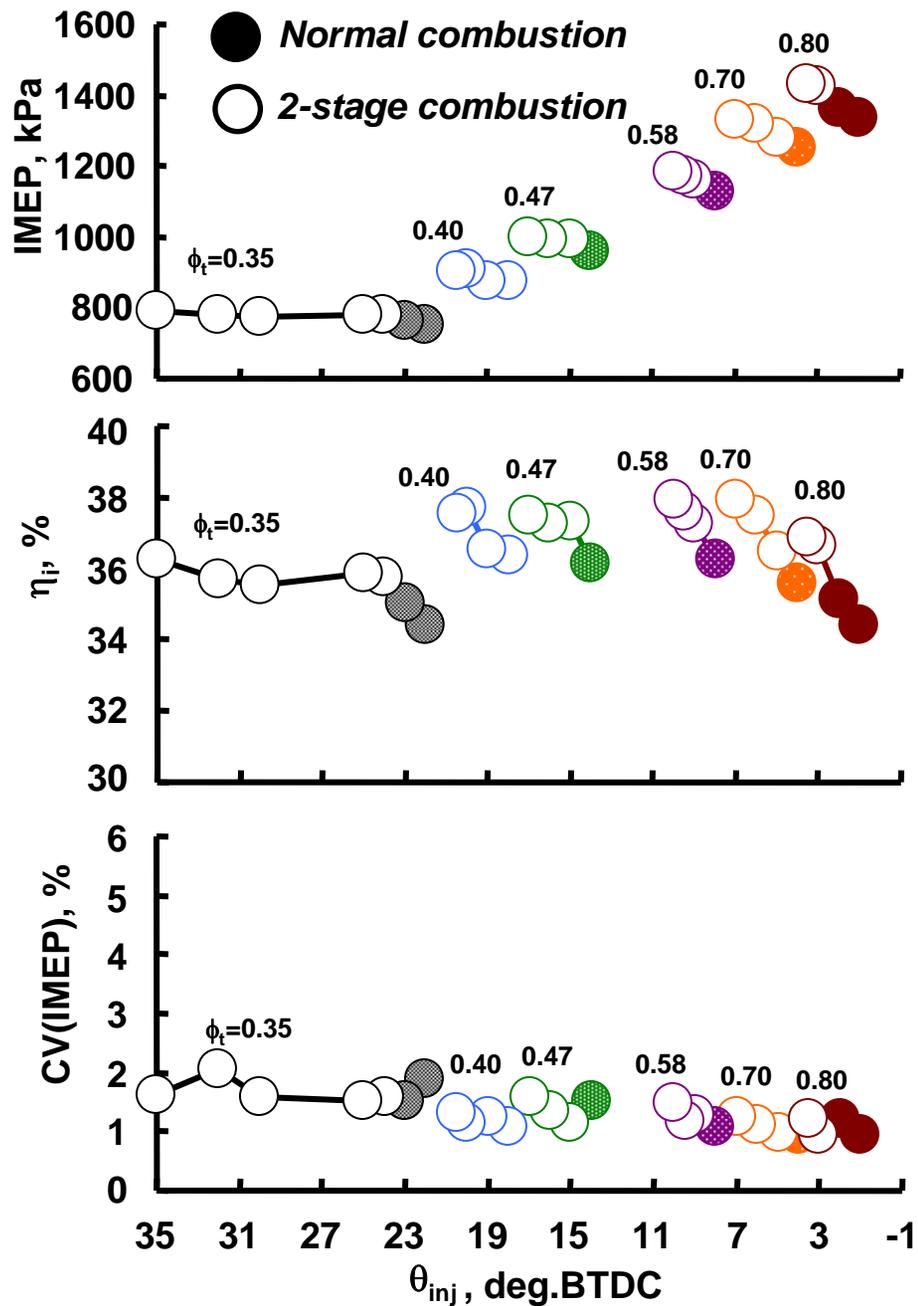
Type2: CO₂-enriched

	CH ₄ [%]	C ₂ H ₆ [%]	C ₃ H ₈ [%]	C ₄ H ₁₀ [%]	H _{lf} [MJ/Nm ³]
NG(13A)	88.9	6.8	3.1	1.2	39.2

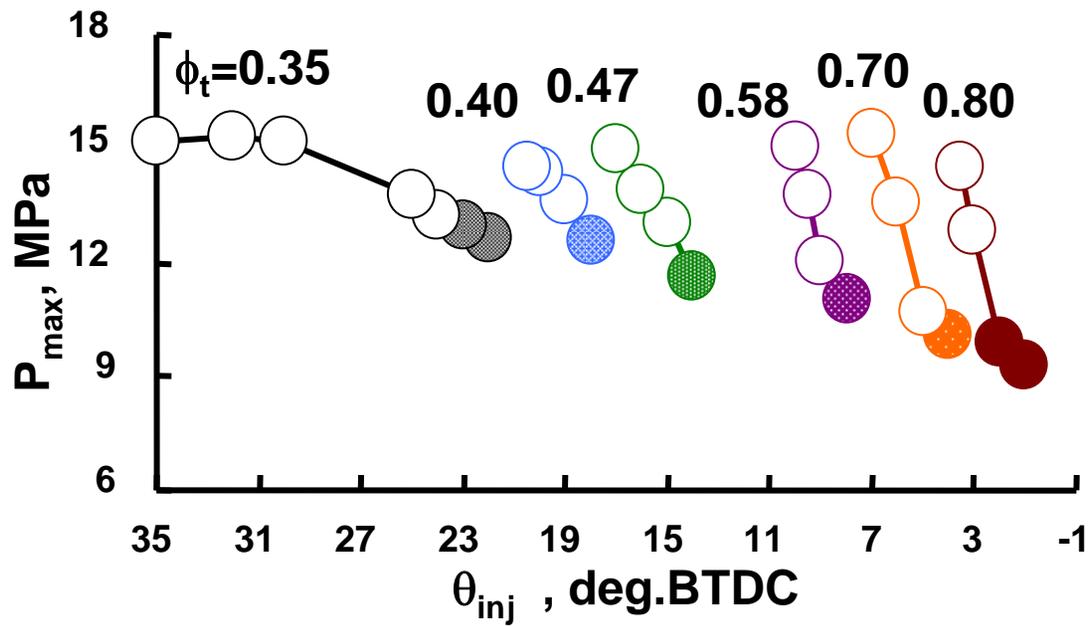
Gas components



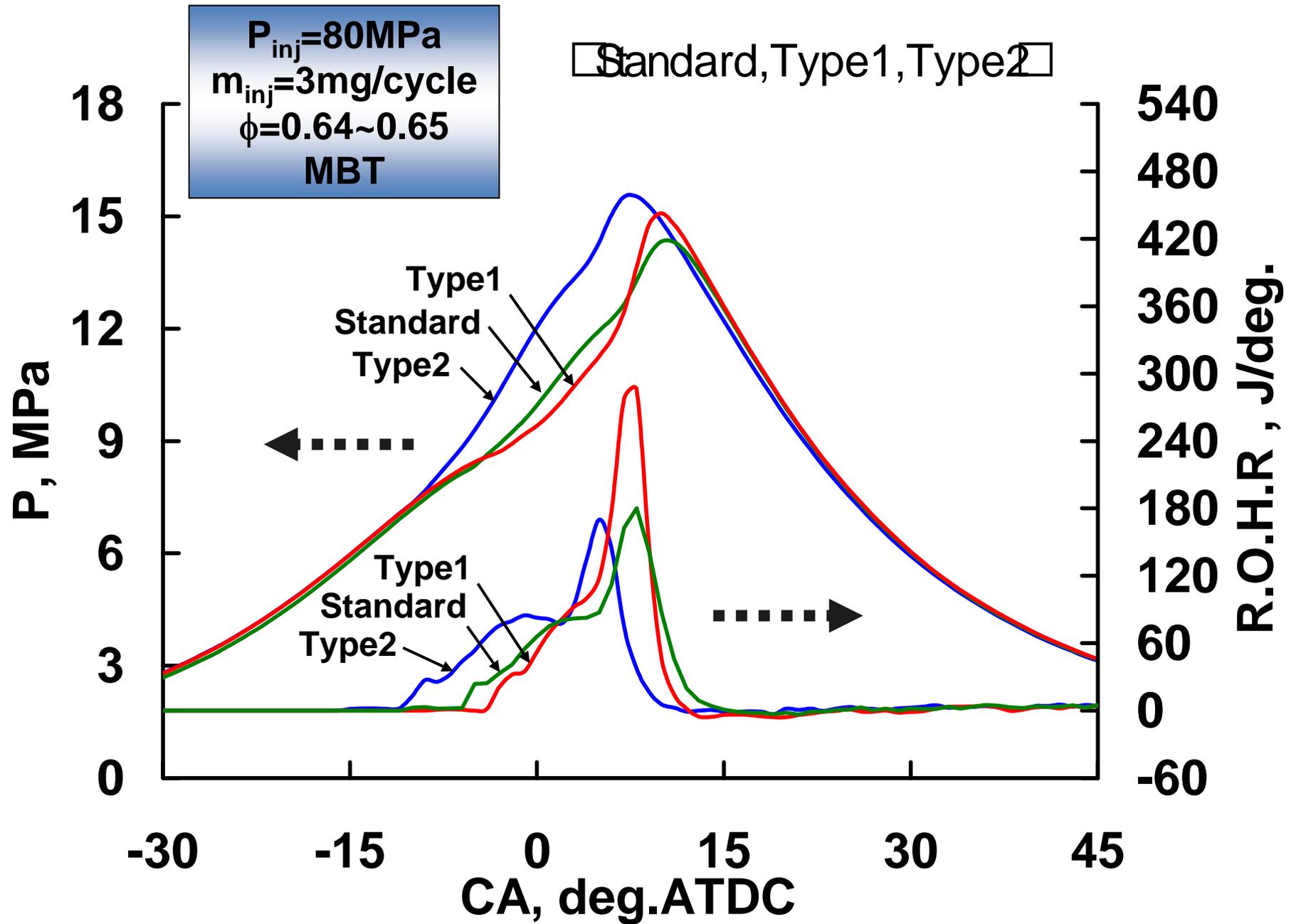
Pressure history and ROHR (Type 1; H2-enriched)



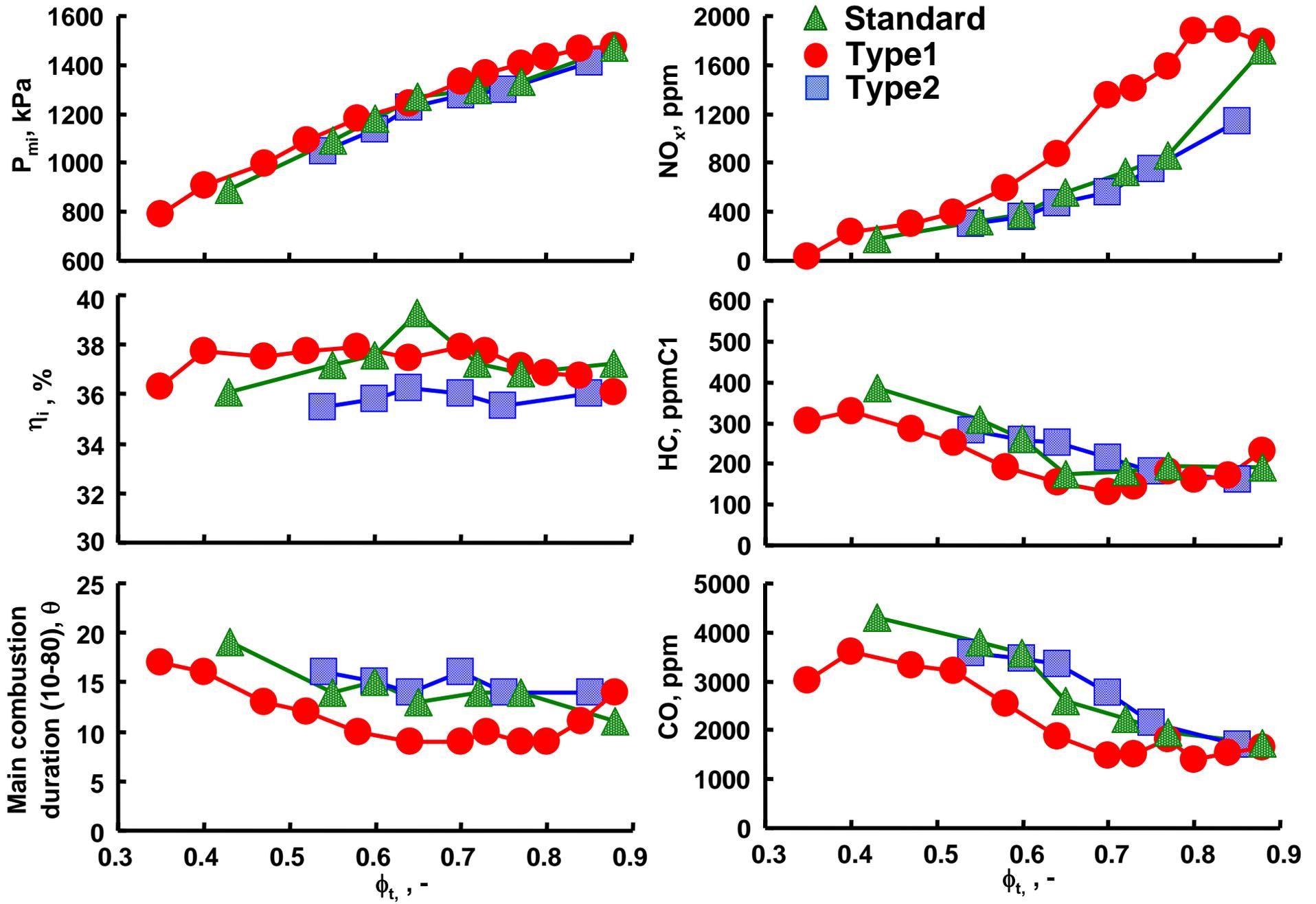
$P_{inj} = 80 \text{ MPa}$, $m_{inj} = 3 \text{ mg/cycle}$, Type1; H₂-enriched



$P_{inj}=80\text{MPa}$, $m_{inj}=3\text{mg/cycle}$, Type1; H2-enriched



Effect of gas component on pressure history and ROHR



Effect of gas component on performance and exhaust emissions

- (1) A broader window of fuel–air equivalence ratio ($\phi=0.42–0.79$) was obtained using high H₂-content producer gas. On the other hand, with low H₂-content producer gas, the optimum window of fuel–air equivalence ratio was narrower ($\phi= 0.52–0.68$).
- (2) Two-stage combustion was an indicator of maximum power conditions as well as a precursor of knock for producer gases. The main combustion (10–80% MFB) with two-stage combustion cycles took less than half the time of normal combustion. In addition, high H₂-content gas reduced the main combustion compared to the case with low H₂-content gas in both normal and two-stage combustion.

Summary